



A METHOD OF CHARACTERISTICS COMPUTER PROGRAM FOR THREE-DIMENSIONAL SUPERSONIC INTERNAL FLOWS

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computer programs flow (shock-free) three dimensional nozzles supersonic flow (internal) axially symmetric flow transonic flow		
The reference-plane method of characteristics is applied to the computation of the supersonic flow in a three-dimensional (3-D) channel such as a propulsion nozzle. The fluid is assumed to be an inviscid ideal gas and the flow is assumed to be shock-free, although it can be rotational. Both the basic equations and the numerical procedures are described, as is the computer program, which was written in FORTRAN IV language for the IBM 370/165		

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20. ABSTRACT (Continued)			
computer. The validity of the computer program was established by computing, in various ways, an axisymmetric nozzle flow as a three-dimensional flow; the numerical results are in good agreement with the results from a well-established computer program for axisymmetric flow.			
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PREFACE

The work reported herein was conducted by the Arnold Engineering Development Center (AEDC), Air Force Systems Command (AFSC). The results presented were obtained by ARO, Inc., AEDC Division (a Sverdrup Corporation Company), operating contractor for the AEDC, AFSC, Arnold Air Force Station, Tennessee. Elton R. Thompson was the Air Force project manager. The work was done under ARO Project No. E32A-POA, and the manuscript was submitted for publication on October 5, 1978.

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1.0 INTRODUCTION

Theoretical calculations of exhaust nozzle performance are often required to aid in the evaluation of engines tested at the Arnold Engineering Development Center (AEDC). In the past, most propulsion nozzles have been axisymmetric and well-established computer programs are available for computing the flow field in such nozzles. However, future tests at AEDC will involve engines with three-dimensional (3-D) exhaust nozzles, and no programs have been available for computing the flow field in 3-D nozzles. Consequently, development of 3-D computer programs for both the transonic and supersonic portions of the flow was initiated. This report describes the supersonic computer program, which is based on the method of characteristics (MOC)....Of course, the computer program described herein is not limited to computation of propulsion nozzle performance, but is also applicable to many other 3-D supersonic internal flows.

Except for the boundary-layer region near the wail, supersonic nozzle flow can be computed with adequate accuracy by assuming the fluid to be inviscid and adiabatic. In addition, most nozzle flows do not contain strong shock waves, so the nozzle performance can be adequately predicted by assuming the flow to be shock-free. However, because of flow phenomena upstream of the nozzle entrance, the flow in propulsion nozzles is often significantly rotational. The rotationality of the flow entering the supersonic region persists throughout the flow field.

In this study, the rotational MOC was chosen as the basis of the numerical analysis. The mathematical theory of characteristics is well established, and many computer programs have been based on the method, particularly for planar and axisymmetric flow. Several programs have been developed to compute the flow over 3-D bodies (e.g., Refs. 1 and 2) and special types of 3-D internal flow have been solved with the method (Ref. 3). However, few attempts have been made to compute general 3-D supersonic internal flows with the MOC.

2,D GOVERNING EQUATIONS

In this section, the governing flow equations and the resulting characteristic equations are presented. These equations are well documented in the literature (e.g., see Ref. 1); therefore, no development will given.

2.1 EQUATIONS OF MOTION

The steady, inviscid, 3-D flow equations for an ideal gas are:

Continuity:

$$u \frac{\partial \rho}{\partial x} + v \frac{\partial \rho}{\partial y} + w \frac{\partial \rho}{\partial z} + \rho \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) = 0$$
 (1)

Momentum:

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} + \frac{L}{\rho} \frac{\partial \rho}{\partial x} = 0$$
 (2)

$$u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} - w \frac{\partial v}{\partial z} + \frac{1}{\rho} \frac{\partial p}{\partial y} = 0$$
 (3)

$$u\frac{\partial w}{\partial x} + v\frac{\partial w}{\partial y} + w\frac{\partial w}{\partial z} + \frac{1}{\rho}\frac{\partial p}{\partial z} = 0$$
 (4)

Energy:

$$u\frac{\partial h}{\partial x} + v\frac{\partial h}{\partial y} + w\frac{\partial h}{\partial z} - \frac{1}{\rho}\left(u\frac{\partial \rho}{\partial x} - v\frac{\partial \rho}{\partial y} + w\frac{\partial \rho}{\partial z}\right) = 0$$
(5)

State:

$$p = \rho RT \tag{6}$$

2.2 CHARACTERISTIC EQUATIONS

The equations of motion give rise to two sets of characteristic surfaces. The defining equations are

$$(uf_x + vf_y + wf_z)^2 = 0$$
 (7)

and

$$(ug_x + vg_y + wg_z)^2 - a_z^2 (g_x^2 - g_y^2 + g_z^2) = 0$$
 (8)

where f(x, y, z) = 0 and g(x, y, z) = 0 are the characteristic surfaces. The first surface is composed of streamlines and the second is the Mach conoid. The equation of a ray, or bicharacteristic, of the Mach conoid may be expressed as

$$dx = (\cos \beta \sin \theta - \sin \beta \cos \theta \cos \delta) dL$$
 (9)

$$dy = \left(\cos\beta\cos\theta\sin\psi - \sin\beta\left(\sin\theta\sin\psi\cos\delta - \cos\psi\sin\delta\right)\right)dL \tag{10}$$

$$dz = (\cos \beta \cos \theta \cos \psi - \sin \beta (\sin \theta \cos \psi \cos \delta + \sin \psi \sin \delta)) dL$$
 (11)

where β is the Mach angle, dL is the distance along the bicharacteristic, δ is a parametric angle, and θ and ψ are related to the velocity vector by

$$u = q \sin \theta \tag{12}$$

$$v = q \cos \theta \sin \psi \tag{13}$$

$$w = q \cos \theta \cos \psi \tag{14}$$

The parametric angle δ lies in a plane normal to the velocity vector and is measured from the plane containing \bar{q} and x. The relationships between the variables are shown in Fig. 1.

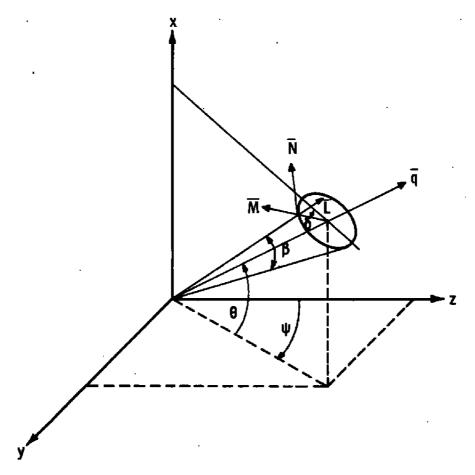


Figure 1. Coordinate system.

2.3 COMPATIBILITY EQUATIONS

The compatibility equations are determined by the flow equations and the requirement that the derivatives in a direction normal to the characteristic surface disappear. The compatibility equation which applies along the Mach conoid is

$$\frac{\cot \beta}{\rho q^{2}} \frac{\partial \rho}{\partial L} + \cos \delta \frac{\partial \theta}{\partial L} + \cos \theta \sin \delta \frac{\partial \psi}{\partial L} - \sin \rho \left(\cos \theta \cos \delta \frac{\partial \psi}{\partial N} - \sin \delta \frac{\partial \theta}{\partial N} \right) = 0$$
(15)

where $\frac{\partial}{\partial L}$ and $\frac{\partial}{\partial N}$ are derivatives along and normal to the bicharacteristic.

The compatibility equations along a streamline are

$$\frac{\gamma}{\gamma - 1} = RdT = \frac{1}{\rho} d\rho \tag{16}$$

and

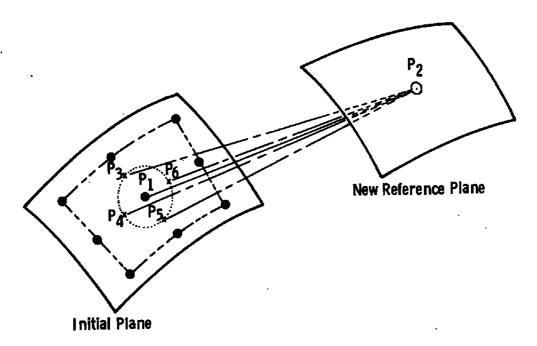
$$\frac{1}{\rho} dp = -q dq \tag{17}$$

3.0 NUMERICAL PROCEDURE

The numerical procedure is similar to the one developed by Strom (Ref. 1) for external flow. The method traces streamlines from a known reference plane to the next reference plane as illustrated in Fig. 2 for a field point. The flow properties at approximately equally spaced points on an initial plane normal to the z axis are assumed known. The reference planes throughout the flow field are assumed to be normal to the z axis.

3.1 METHOD OF SOLUTION

A new reference plane is located a distance dz from the initial plane. This distance must be determined such that the Courant-Friedrichs-Lewy (C-F-L) stability conditions are satisfied (Refs. 1 and 4). The C-F-L stability conditions are satisfied if dz is smaller than the minimum intersection distance of the Mach conoids from the initial points.



- Known Points in Initial Plane
- O Point in New Reference Plane (P2)
- x Points in Initial Plane on Bicharacteristics from P2
- ---- Streamline
- --- Bicharacteristic
- --- Domain of Dependence of Difference Network
- ---- Domain of Dependence of Differential Equations

For the C-F-L stability conditions to be satisfied, the domain of dependence of the differential equations must be contained within the domain of dependence of the difference network.

Figure 2. Field point network.

The intersection of a streamline from a point P_1 in the initial plane with the new reference plane locates point P_2 . Four bicharacteristics, 90 deg apart, from P_2 to the initial plane yield points P_3 , P_4 , P_5 , and P_6 .

The properties at P_1 and eight surrounding neighbors in the initial plane are surface fitted. The flow conditions at points P_3 - P_6 are evaluated from the surface fit. The compatibility equations are applied

along the bicharacteristics and the streamline to obtain the flow conditions at P_2 . This procedure is iterated until the flow conditions at P_2 converge. When all points on the new plane are determined, the new plane becomes the initial plane for the next calculation.

3.2 WORKING EQUATIONS

Several of the computational steps are the same for both field points and body points. These common phases of the procedure will be discussed first. Then the computational steps required for field and body points will be presented individually.

3.2.1 Common Procedures

The surface fit of the flow properties at P_1 and eight neighboring points in the initial plane is made once in the iteration procedure to obtain P_2 and its properites. The fit chosen is a spline surface fit (Ref. 5) which fits a variable was a function of x and y:

$$w(x,y) = a_0 + a_1 x + a_2 y + \sum_{i=1}^{9} b_i r_i^2 \ln r_i^2$$
 (18)

where

$$r_i^2 = (x - x_i)^2 + (y - y_i)^2$$

Five variables are fit: p, p, q, θ , and ψ . The surface fit is used to evaluate the variables at $P_3 - P_6$. The partial derivaties $\frac{\partial}{\partial x}$ and $\frac{\partial}{\partial y}$ are also evaluated using this fit:

$$\frac{\partial w}{\partial x} = a_1 + 2 \sum_{i=1}^{9} b_i \left(1 + \ln r_i^2 \right) \left(x - x_i \right)$$
 (19)

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$$\frac{\partial w}{\partial y} = a_2 + 2 \sum_{i=1}^{9} b_i \left(1 + \ln r_i^2 \right) (y - y_i)$$
 (20)

The derivatives $\frac{\partial \theta}{\partial N}$ and $\frac{\partial \psi}{\partial N}$ used in the compatibility equation along a bicharacteristic must be obtained. The procedure for evaluating them is the same; therefore, only the procedure to obtain $\frac{\partial \theta}{\partial N}$ will be given. Write $\frac{\partial \theta}{\partial N}$ as

$$\left(\frac{\partial \theta}{\partial N}\right)_{i} = \left(\frac{\partial \theta}{\partial x}\right)_{i} \left(\frac{\partial x}{\partial N}\right)_{i} + \left(\frac{\partial \theta}{\partial y}\right)_{i} \left(\frac{\partial y}{\partial N}\right)_{i} + \left(\frac{\partial \theta}{\partial z}\right)_{i} \left(\frac{\partial z}{\partial N}\right)_{i}$$
(21)

The derivatives $\frac{\partial \theta}{\partial x}$ and $\frac{\partial \theta}{\partial y}$ are obtained from the surface fit. Then, $\frac{\partial \theta}{\partial z}$ is obtained by writing the equation as a difference equation and solving for $\frac{\partial \theta}{\partial z}$:

$$\theta_2 - \theta_i = \left(\frac{\partial \theta}{\partial x}\right)_i \left(x_2 - x_i\right) + \left(\frac{\partial \theta}{\partial y}\right)_i \left(y_2 - y_i\right) + \left(\frac{\partial \theta}{\partial z}\right)_i dz$$
 (22)

The derivatives normal to the bicharacteristic are obtained from the coordinate transformation as

$$\left(\frac{\partial x}{\partial N}\right)_{i} = -\cos\theta\sin\delta_{i} \tag{23}$$

$$\left(\frac{\partial y}{\partial N}\right)_{i} = \sin\theta \sin\psi \sin\delta_{i} + \cos\psi \cos\delta_{i} \tag{24}$$

$$\left(\frac{\partial z}{\partial N}\right)_{i} = \sin\theta \cos\psi \sin\delta_{i} - \sin\psi \cos\delta_{i} \tag{25}$$

The final form of $\frac{\partial \theta}{\partial N}$ becomes

$$\left(\frac{\partial\theta}{\partial N}\right)_{i} = \left(\frac{\partial\theta}{\partial x}\right)_{i} \left(\frac{\partial x}{\partial N}\right)_{i} + \left(\frac{\partial\theta}{\partial y}\right)_{i} \left(\frac{\partial y}{\partial N}\right)_{i} \\
- \left[\theta_{i} + \left(\frac{\partial\theta}{\partial x}\right)_{i} \left(x_{2} - x_{i}\right) + \left(\frac{\partial\theta}{\partial y}\right)_{i} \left(y_{2} - y_{i}\right)\right] \left(\frac{\partial z}{\partial N}\right)_{i} dz + \theta_{2} \left(\frac{\partial z}{\partial N}\right)_{i} dz$$
(26)

For the first iteration, the flow properties at P_2 are assumed to be the same as at P_1 . Thereafter, the last computed values are used. In the sections on the field point and body point, the average values of flow properties are the averages of the two points involved in the calculation (for example, $\theta = (\theta_1 + \theta_2)/2$).

3.2.2 Field Point Routine

Given an initial field point P_1 and eight neighboring points in the initial plane (Fig. 2), spline surface fits of p, p, q, 0, and ψ as functions of x and y are made. The iteration for the point P_2 and its flow properites consists of the following steps.

Step 1.

The intersection of the streamline from P_1 with the new reference plane locates the new field point P_2 .

$$x_2 = x_1 - \sin\theta \, dz/(\cos\theta \cos\psi) \tag{27}$$

$$y_2 = y_1 + \sin \psi \, dz/\cos \psi \tag{28}$$

$$z_2 = z_1 + dz \tag{29}$$

Initially θ and ψ are the values at P_1 . Successive iterations use the average of θ and ψ at P_1 and P_2

Step 2

Four bicharacteristics extended from P_2 to the initial plane give the base points P_3 , P_4 , P_5 , and P_6 . The flow properties at P_2 are

assumed to be the same as those at P_1 for the first iteration. Thereafter, the flow properties at P_2 are the last values computed. The bicharacteristics are located at the parametric angles $\delta = 0$, $\frac{\pi}{2}$, π , and $\frac{3\pi}{2}$. The equations for the base points are

$$x_i = x_2 - (\cos \beta \sin \theta + \sin \beta \cos \theta \cos \delta_i) dL_i$$
 (30)

$$y_i = y_2 - \left[\cos \beta \cos \theta \sin \psi - \sin \beta \left(\sin \theta \sin \psi \cos \delta_i - \cos \psi \sin \delta_i\right)\right] dL_i$$
 (31)

$$z_i = z_i \tag{32}$$

$$dL_{i} = dz / \left[\cos \beta \cos \theta \cos \psi - \sin \beta \left(\sin \theta \cos \psi \cos \delta_{i} + \sin \psi \sin \delta_{i} \right) \right]$$
 (33)

For the first iteration, the angles β , θ , ψ , and δ are those at P_2 . Successive iterations use the average of the values at P_2 and P_4 .

Step 3

The compatibility equations along the bicharacteristics are solved for p, θ , and ψ at P₂. Only three of the bicharacteristics are required; however, to improve accuracy, four solutions are obtained using three bicharacteristics at a time. The results of the four solutions are averaged to obtain the values of p, θ , and ψ . The compatibility equation in difference form is

$$\frac{\cot \beta_{i}}{\rho_{i} q_{i}^{2}} \left(P_{2} - P_{i}\right) + \cos \delta_{i} \left(\theta_{2} - \theta_{i}\right) + \cos \theta_{i} \sin \delta_{i} \left(\psi_{2} - \psi_{i}\right) + \sin \beta_{i} \left(\cos \theta_{i} \cos \delta_{i} \left(\frac{\partial \psi}{\partial N}\right)_{i} - \sin \delta_{i} \left(\frac{\partial \theta}{\partial N}\right)_{i}\right) dL_{i} = 0$$
(34)

......

The equation contains the three unknows P_2 , θ_2 , and ψ_2 . The compatibility equations using P_3 , P_4 , and P_5 are solved simultaneously for P_{21} , θ_{21} , and ψ_{21} - similarily, (P_4, P_5, P_6) , (P_5, P_6, P_3) , and (P_6, P_3, P_4) are used to obtain values of p, θ , and ψ . Thus, $P_2 = (P_{21} + P_{22} + P_{23} + P_{24})/4$. In the compatibility equation, β_1 , ρ_1 , q_1 , and δ_1 are the average of the values at P_2 and P_1 .

The variables ρ_2 , T_2 , and q_2 are obtained from the compatibility equations along the streamline. The flow along a streamline without shocks is isentropic. Therefore, the equations integrate to the following forms for an ideal gas:

$$T_{2} = T_{1s} \left(\frac{p_{2}}{p_{1s}} \right)^{\frac{\gamma - 1}{\gamma}}$$
(35)

$$\rho_2 = R T_2 / P_2 \tag{36}$$

$$q_2 = \sqrt{2} \frac{y}{y-1} (T_{1s} - T_2)$$
 (37)

where T_{ts} and p_{ts} are the stagnation values for the streamline.

Step 4

The preceding steps are repeated until the flow conditions at P_2 converge. If there is no convergence after 25 iterations, the results are checked with a reduced convergence criterion. If this is satisfied, the point is accepted and a message printed. Otherwise, the program terminates.

3.2.3 Body Point Routine

Given the properties of an initial body point P₁ and those of eight neighboring points on the initial plane (Fig. 3), spline surface fits are made. The body surface is assumed to be given by

$$B(x, y, z) = 0 (38)$$

where B is either a known function or a surface fitting element in the region of the body point. The iteration for the new body point P₂, in the new reference plane, and its flow properties consists of the following steps:

Step 1

The new body point P_2 is located at the intersection of a plane through P_1 , defined by the body unit normal and the unit velocity vector tangent to the body at P_1 , with the body surface at the new reference plane. This requires the simultaneous solution of the following equations:

$$B(x, y, z) = 0 (39)$$

and

$$(n_3 \cos \theta \cos \psi - n_1 \cos \theta \sin \psi) (x - x_1) + (n_1 \sin \theta - n_2 \cos \theta \cos \psi) (y - y_1) = (n_3 \sin \theta - n_1 \cos \theta \sin \psi) dz$$

$$(40)$$

where n_1 , n_2 , and n_3 are unit normals to the body surface. The first iteration uses the values of θ , ψ , n_1 , n_2 , and n_3 , at P_1 . Successive iterations use the averages of the properties at P_1 and P_2 .

Step 2

This step is similar to Step 2 of the field point routine. However, only three bicharacteristics are used for the body point calculations. The parametric angles used are

$$\delta_3 = \arccos\left(-n_1\sin\theta\cos\psi + n_2\cos\theta - n_3\sin\theta\sin\psi\right) \tag{41}$$

$$\delta_4 = \delta_3 - \pi/2 \tag{42}$$

$$\delta_5 = \delta_3 - \pi/2 \tag{43}$$

Step 3

The compatibility equations along two bicharacteristics are solved simultaneously with the condition for flow tangency to the surface at P_2 . The equation for flow tangency, which provides an additional relationship between θ_2 and ψ_2 may be expressed as

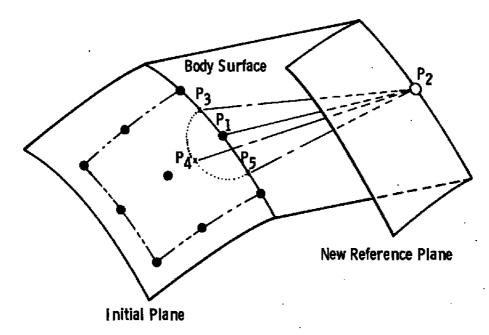
$$n_{12}\cos\theta_2\cos\psi_2 + n_{22}\sin\theta_2 + n_{32}\cos\theta_2\sin\psi_2 = 0$$
 (44)

where n_{12} , n_{22} , and n_{32} are unit normals to the body at P_2 . A Newton-Raphson routine is used to solve this system of equations. The base points P_3 and P_4 are used to obtain P_{21} , θ_{21} , and ψ_{21} ; P_3 and P_5 are used to obtain P_{22} , θ_{22} , and ψ_{22} . These two results are averaged to obtain the values at P_2 ($P_2 = (P_{21} + P_{22})/2$).

The compatibility equations along the streamline are solved the same way as for the body point yielding ρ_2 , q_2 , and T_2 .

Step 4

The iteration procedure for the body point is the same as the procedure used for the field point.



- Known Points in Initial Plane
- Point in New Reference Plane and Body Surface (P2)
- × Points in Initial Plane on Bicharacteristics from P2
- Streamline
- --- Bicharacteristic
- --- Domain of Dependence of Difference Network
- ----- Domain of Dependence of Differential Equations

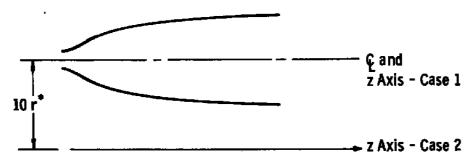
Figure 3. Body point network.

3.2.4 Computer Program

The preceding equations were programmed in FORTRAN IV language for solution on an IBM 370/165 computer. A description and listing of the program is given in Appendix A, and an example problem is given in Appendix B. The program requires a storage capacity of approximately 192,000 bytes.

4.0 RESULTS AND DISCUSSION

The present 3-D MOC program was evaluated by computing the flow in a typical axisymmetric nozzle. With γ = 1.24 and uniform flow in the throat, the nozzle produces an exit Mach number of 4.1. The 3-D MOC computations were done in three different ways (see 4).



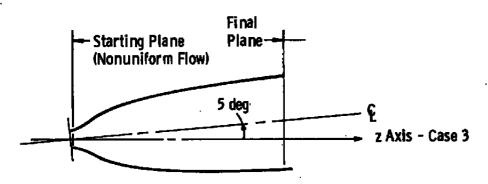


Figure 4. Geometry for test cases.

- <u>Case 1</u> The z axis was aligned with the geometric centerline of the nozzle.
- Case 2 The z axis was parallel to the nozzle centerline but was displaced by a distance of 10 nozzle throat radii; thus, the z axis for the flow field is completely outside the nozzle.

Case 3 - The z axis was rotated 5 deg relative to the nozzle centerline. In this case, the flow in the starting plane is nonuniform and was obtained by interpolation from the flow field predicted for case 1.

The predicted wall Mach number distribution for case 1 is shown in Fig. 5 along with the predictions of the Lockheed axisymmetric MOC computer program (Ref. 6) which is well verified and widely used. The results from the two programs are in good agreement. At the nozzle exit plane, the circumferential variation of wall Mach number calculated by the 3-D MOC program is much less than one percent.

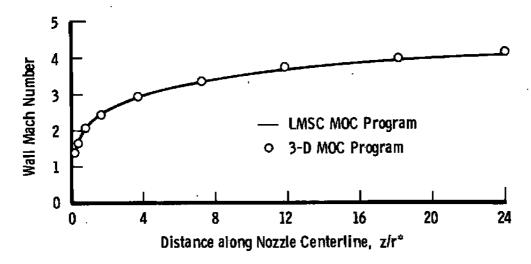


Figure 5. Results for z axis aligned with nozzle centerline.

The results of the three 3-D computations are compared in Fig. 6 where it is seen that the three predicted wall Mach number distributions are essentially identical.

These computations of axisymmetric nozzle flow, done the "hard way" with the 3-D MOC program, indicate that the program is acceptably accurate and is capable of computing the supersonic flow in complex configurations.

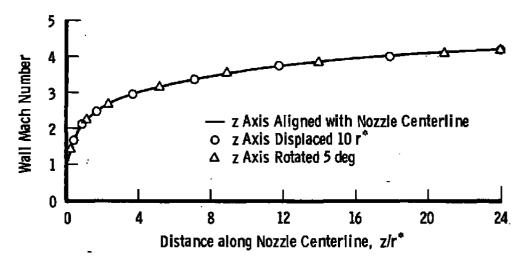


Figure 6. Results of 3-D MOC program.

In each of the test cases, 346 streamlines were traced throughout the flow field. For cases 1 and 2, 78 reference planes were computed which required a CPU time of approximately 25 min. Fewer reference planes were computed for case 3, with a corresponding reduction in CPU time.

5.0 CONCLUDING REMARKS

The results obtained for an axisymmetric nozzle with the 3-D MOC computer program are acceptably accurate. However, additional verification of the program is clearly required. The predictions of the code should be compared with experimental results for 3-D supersonic flows, whenever adequately detailed experimental results become available.

Two extensions of the 3-D MOC computer program are recommended. First, the program should be modified to include a constant-pressure free boundary condition for part of the flow field. This modification would permit the computation of the exhaust plume from a 3-D nozzle. The second recommended modification is the inclusion of shock formation, both within the nozzle and in the exhaust plume.

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APPENDIX A DESCRIPTION OF COMPUTER PROGRAM

DESCRIPTION OF ROUTINES

NAME	FUNCTION `
MAIN	CALLS CARDIN. INGEOM. INPUT. AND THREED
BDYF IT	CURVE FITS BODY IN AREA OF INTEREST
BODY	BODY POINT ROUTINE
CARDIN	READS AND PRINTS INPUT CARD IMAGES
•	
CUT	INTERPOLATES THE BODY GEOMETRY IN CURRENT PLANE
DELTAF	COMPUTES THE BICHARACTERISTIC ANGLE DELTA
TRIG	COMPUTES MIN. DIST. OF CHARACTERISTIC INTERSECTIONS
FIELD	FIELD POINT ROUTINE
FIND	LOCATES POINTS NEAREST TO GIVEN POINT
FINDBP	LOCATES BODY GEOMETRY POINT NEAREST GIVEN POINT
FIT	SURFACE FIT ROUTINE
IDENT	WRITES HEADER AND TRAILER LABELS ON PLOTS
INGEOM	READS GEOMETRY INPUT
TUPUT	READS STARTING PLANE INPUT
NE IGH	LOCATES (OR READS) 8 NEIGHBORS OF EACH INPUT POINT
NEWRAP	NEWTON-RAPHSON ROUTINE
NORMAL.	COMPUTES THE NORMAL VECTOR TO THE BODY SURFACE
TUSTUG	CONTROLS PRINTED. PLOTTED. AND TAPE OUTPUT
SIMQ	SOLVES SYSTEM OF SIMULTANEOUS LINEAR EQUATIONS
SOL VBP	SOLVES FOR THE LUCATION OF A BODY POINT
SORT	SORT ROUTINE
THREED	CONTROLS THE 3-D CALCULATIONS
	,

INPUT NOMENCLATURE

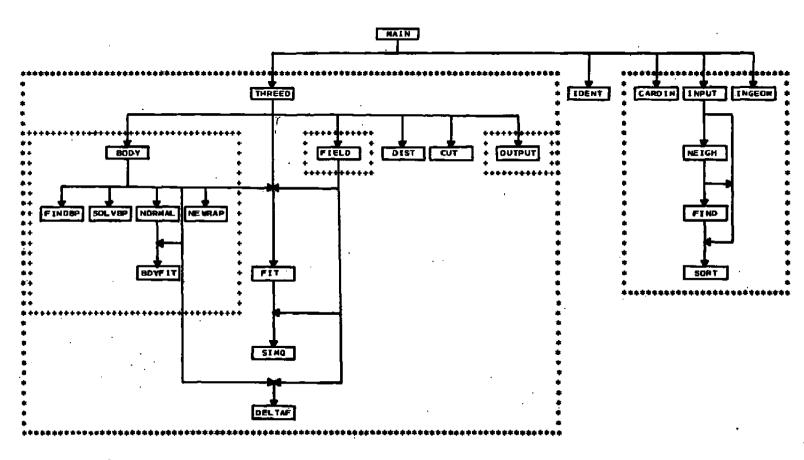
```
RATIO OF SPECIFIC HEATS
G
HEAD
          PROBLEM DESCRIPTION
          SPECIAL PRINT FLAGS
                               =0 NO PRINT: =1 PRINT
(I) DUBG()
            IDBUG( 1) PRINT INPUT GEOMETRY
            IDBUG( 2) PRINT FINAL GEGMETRY
            IDBUG( 3) PRINT INITIAL PLANE INPUT
            IDBUG( 4) PRINT FINAL INITIAL PLANE DATA
            IDBUG( 5) PRINT NEIGHBORS
            IDBUG(11) PRINT NORMAL CALCULATION
          INITIAL PLANE DATA TYPE
EMV
                                     THETA
                                                 PS I
            IMV=0
                         Q
                                                 PS I
            I MV=1
                         М
                                     THETA
            IMV=2
                                       U
          NEIGHBOR CONTROL
INEIGH
            INEIGH=0 NEAREST POINTS ARE NEIGHBORS
                       SPECIAL COMPUTATION OF NEIGHBORS
            INE IGH=1
                       READ NEIGHBORS FROM CARDS
            INEIGH=2
              IF ITYPE=0 AND INEIGH=0. INEIGH IS SET TO 1
          ±0 NC PLOTS: =1 PLCTS
IPLOT
          COORDINATE SYSTEM FOR BODY POINTS AT THIS STATION
IT(I)
            IT(I)=0 RECTANGULAR COORDINATES
            IT([)=1
                      PCLAR CCCRDINATES
                     PCLAR CCORDINATES - AXISYMMERIC
            IT(I)=2
          COORDINATE SYSTEM FOR STARTING PLANE INPUT
ITYPE
            ITYPE=0 PCLAR COCRDINATES - AXISYMMETRIC
                      PCLAR COURDINATES
            t TYPE=1
            ITYPE=2 RECTANGULAR COURDINATES
          FLOW FIELD TAPE CUTPUT IT11=0 NO TAPE; IT11=1 TAPE
1711
          BODY DATA TAPE OUTPUT IT12=0 NC TAPE: [T12=1 TAPE
FT12
          NO. CF BODY PCINTS AT THIS STATION
IV(I)
          MAXIMUM NO. OF PLANES TO BE COMPUTED
XAML
          PRINT EVERY JPT PLANES
JPT
          =0 INPUT FOR FIELD PCINT; =1 INPUT FOR BODY POINT
NBT
NE(J<sub>1</sub>K)
          THE J-TH NEIGHBOR OF THE K-TH POINT
          TOTAL NO. OF POINTS IN STARTING PLANE
NPTS
           IF ITYPE=0 NO. OF POINTS ON A RAY
          NO. OF RAYS IF ITYPE=0; OTHERWISE NOT USED
NRAYS
          NO. OF STATIONS OF BODY GEOMETRY INPUT
NS.
```

INPUT NOMENCLATURE (CONT.)

P(I)	PRESSURE		
PSI(1)	ANGLE SHOWN IN FIG. 1: OR V IF IMV=2		
P70(1)	TOTAL PRESSURE AT POINT (IF 0.0. SET TO PTO)		
PTO	TOTAL PRESSURE FOR IRROTATIONAL FLOW		
Q(I)	VELOCITY IF IMV=0; MACH NUMBER IF IMV=1; W IF IMV=2		
RO	GAS CONSTANT		
THETALL)	ANGLE SHOWN IN FIG. 1: OR U IF IMV=2		
TTO	TOTAL TEMPERATURE		
X(1)	POINT IN STARTING PLANE		
	X IF ITYPE=2; R IF ITYPE=0 OR 1		
XC(J.[]	BODY POINT X IF IT(I)=0; R IF IT(I)=1 OR 2		
Y(I)	POINT IN STARTING PLANE .		
	Y IF ITYPE=2; ANGLE IF [TYPE=0 OR 1		
YC(J+1)	BODY POINT Y IF IT(I)=0; ANGLE IF IT(I)=1 OR 2		
ZC(E)	Z LOCATION OF BODY STATION		
ZMAX	MAXIMUM Z LOCATION FOR CALCULATIONS		
ZO	Z LOCATION OF STARTING PLANE		

INPUT CARDS IN ORDER READ

CARD	FORMAT	CONTENTS
1	(20A4)	(HEAD([].[=1.20]
2	(1108)	(IDBUG(I).I=1.80)
3	(15)	NS ;
4	(215.E10.0)	[V(1).IT(I).ZC(I)
5	(8E10.0)	(()) VI. I=L. (I.L) OY. (I.L) OX)
	READ (CARDS 4 AND 5 NS TIMES
€	(4E10.0)	G.PTO.TTO.RO
7	(2E10.0.1015)	ZO.ZMAX.ITYPE.IMV.NPTS.NRAYS.JMAX.
		JPT.IPLOT.IT11.IT12.INEIGH
a	(7E10.0.15)	X(1).Y(1).P(1).Q(1).THETA(1).PS1(1).
		PTG(I)+NBP READ NPTS CARDS
9	(9110)	(K.(NE(J.K).J=1.8).I=1.NPTS)
	· READ	CARD 9 ONLY IF INEIGH=2



***** PRIMARY OVERLAY ++++* SECONDARY OVERLAY

```
THREE DIMENSIONAL DUCT FLOW
C
                                                SRR00886
C
           SIMPLIFIED VERSION WITH FOLLOWING ASSUMPTIONS
C
              NO INTERNAL SHOCKS
¢
              IDEAL GAS
C
                     FUNCTION
           UNIT
C
            5
                      CARD INPUT
C
            6
                       PRINTED GUTPUT
C
                       PLOTTED OUTPUT
            10
C
            11
                      FLOW FIELD OUTPUT
C
                       BODY OUTPUT
            12
C
            8
                       WORK DATA SET
C
          OVERLAY STRUCTURE
C
            OVERLAY A
¢
             INSERT CARDIN, INGEOM, INPUT, NEIGH, FIND, SORT
C
            DVERLAY A
¢
             INSERT THREED, CUT.FIT.DIST.SIMQ.DELTAF
¢
            OVERLAY B
C
             INSERT FIELD
C
            OVERLAY B
C
             INSERT BODY . FINDSP . SOLVBP . NORMAL . BDYFIT . NEWRAP
C
            OVERLAY B
C
             INSERT DUTPUT
      COMMON /TITLE/HEAD(20)
      COMMON/IDEBUG/IDBUG(80)
      COMMON /STAG/DUMNY(1207) . IPLOT . IT11 . IT12
      DATA ISTRP/0/
    1 FORMAT(20A4)
    2 FORMAT(8011)
      CALL CARDIN
   20 CONTINUE
      READ(8.1.END=99)HEAD
      READ(8.2) [DBUG
      CALL INGEOM
      CALL INPUT
                      GO TO 21
       IF(IPLOT.EQ.O)
      IF(ISTRP.NE.O)
                        GO TO 21
      I STRP=1
      CALL IDENT(1)
   21 CONTINUE
      CALL THREED
      GO TO 20
   99 CONTINUE
       [F([STRP.NE.O) CALL | DENT(2)
       STOP
      END
```

```
SUBROUTINE BDYFIT(A.B.C.XB.YB.I.IT)
      IMPLICET REAL +8(A-H.O-Z)
      REAL *4 DUMMY(5051) . XB(50) . YB(50)
      COMMON /GEOM/DUMMY.NP
C
          I T=1
                    X=C
C
          I T=2
                    Y=C
C
          I T=3
                    AX+BY=C
C
           I T=4
                    (X-A) **2+(Y-B) **2=C
      IM1=[-1
      IF(I.EQ.1)
                   IM1=NP
      XI=XB([M1]
      Y1=YB(IM1)
      X2=XB([)
      Y2=YB(I)
      191=1+1
      IF(I.EQ.NP)
                    IP1=1
      X3=XB(IP1)
      Y3=Y8(IP1)
      [F({X1.NE.X2}.OR.(X1.NE.X3}) GO TO 21
      I T=1
      A=1.0
      B=0.0
      C≔X2
      RETURN
   21 CONTINUE
      IF((Y1.NE.Y2).OR.(Y1.NE.Y3)) GO TO 22
      £ T=2
      A=0.0
      B=1.0
      C=Y2
      RETURN
   22 CONTINUE
      R1=X1**2+Y1**2
      R2=X2++2+Y2++2
      R3=X3++2+Y3++2
      DX21=2.D0+(X2-X1)
      DY21=2.00*(Y2-Y1)
      DX32=2.D0+(X3-X2)
      DY32=2.D0*(Y3-Y2)
     'IF(DX21.NE.O.DO) GO TO 23
      DX21=2.D0*(X3-X1)
      DX32=-DX32
      DY21=2.00+(Y3-Y1)
      DY32=-DY32
      H=R2
      R2=R3
      R 3=H
      GO TO 24
   23 CONTINUE
      IF(DX32.EQ. 0.D0) GO TO 24
```

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```
IF((DY21/DX21).NE.(DY32/DX321) GO TO 24
   I T=3
  A=-DY21/DX21
  8=1.00
  C=Y1+X1*A
  RETURN
24 CONTINUE
   1T=4
   A=(R2-R1)/DX21
   B=R3-R2
  C=DY21/DX21
  H=0 Y 32
   IF(DX32.EQ.0.D0) GO TO 25
   8=8/DX32-A
   H=H/DX32-C
25 CONTINUE
   8=8/H
   A=A-B+C
   C=R1-2.D0+(A+X1+B+Y1)
   C=C+B++2+A++2
   RETURN
   END
```

```
SUBROUTINE BODY(I)
 IMPLICIT REAL+8(A-H,D-Z)
 REAL *4 ZD.XN(1000).YN(1000).PN(1000).RN(1000).QN(1000).
*PSN(1000).ZE.X(1000).Y(1000).P(1000).RHQ(1000).
*Q{1000},THETA{1000},XB(50),YB(50),XBO(50),YBO(50),
*TN(1000) .PSI(1000)
 COMMON /NVALU/ZD.XN.YN.PN.RN.QN.TN.PSN
 COMMON /VALUE/ZE.X.Y.P.RHO.Q.THETA.PSI.N
 COMMON /BCUT/XB +YB
 COMMON /OCUT/XBD.YBC
 COMMON /DGAS/DZ.G.RO.GM1.GM1H.GM1G.GGM1.GP1.GPGM
 COMMON/IDEBUG/IDBUG(80)
 REAL #8 N11.N21.N31.N12.N22.N32.N1.N2.N3
 COMMON /POINT/X1.Y1.P1.R1.Q1.T1.TH1.P51.BE1.X2.Y2.P2.
*R2.Q2.T2.TH2.PS2.BE2.P2Q.T2O.PSQ.OEL(4).PI(4).THI(4).
*P[[(4),BEI(4),XI(4),YI(4),DEI(4),DX(4),DY(4),DL(4),
*PP(5.4).T12.P12.B12.T2I(4).P2I(4).B2I(4).D2I(4)
 COMMON /FLDBDY/SINT12, COST12, SINP12, CDSP12, SINB12.
*CQSB12.SIND2I(4).CQSD2I(4).SINT2I(4).CQST2I(4).
*SINP2[(4).COSP2I(4).SINB2[(4).COSB2I(4).DXON(4).
*DYDN(4).DZDN(4).DTDX(4).DTDY(4).DTDZ(4).DPDX(4).
*DPDY(4)*DPDZ(4)*DER(2.5)*AL(3.4)*CR(4)*AM(3.3)*CM(3.4)
1 FORMAT( O FAILED IN BODY AT POINT . I5.5X. Z1= ...
#1PE12.5.5x, 'DZ='.E12.5//5X.'X1='.E12.5.5x.'Y1='.E12.5.
*5X.*P1=*.E12.5.5X.*T1=*.E12.5.5X.*PS1=*.E12.5/5X,*X2=*
*.El2.5.5X.'Y2='.El2.5.5X.'P2='.El2.5.5X.'T2='.El2.5.5X
*• 'PS2=',E12.5/45X,'P20=',E12.5,4X.'T20=',E12.5.4X..
*'P520=',E12.5//)
 x1=x(I)
 Y1=Y(I)
 P1=P(I)
 R1 = RHO(1)
 Q1=Q\{1\}
 TH1=THETA([)
 PS1=PSI(I)
 T1=P1/(R0+R1)
  SINT1=DSIN(TH1)
 COST1=0COS(TH1)
 SINP1=DSIN(PS1)
 COSP1=DCOS(PS1)
 BE1=DARS[N(DSQRT(G*P1/R1)/Q1)
 P2=P1
 R2=R1
 Q2=Q1
  TH2=TH1
 PS2=PS1
  T2=T1
 BE 2=BE 1
 CALL FINDBP(X1.Y1.XBD.Y80.IBP1)
 CALL BDYFIT(A1.B1.C1.XB0.YB0.IBP1.IT1)
```

```
CALL BDYF I T(A2 , 82 , C2 , X8 , Y8 , I8P1 , IT2)
  CALL NGRMAL(X1.Y1.ZE.A1.B1.C1.N11.N21.N31.IT1.IBP1)
  CALL NORMAL(X1,Y1,ZE+DZ,A2,82,C2,N12,N22,N32,IT2,IBP1)
  DEL(1)=DARCOS(-N11+SINT1+COSP1+N21+COST1-N31+SINT1+
  *SINP1)
   IF(N31-LT.0.00) DEL(1)=6.28318530700-DEL(1)
  DEL(2)=DEL(1)-1.57079632700
   IF(DEL(2).LT.0.D0) DEL(2)=6.283185307D0+DEL(2)
  DEL(3)=DEL(1)+1.570796327D0
   1F(DEL(3).GE.6.283185307D0)
  *DEL(3) =DEL(3)-6.283185307D0.
   DO 21 IT=1.4
   THI(IT)=TH1
   PII(IT)=PS1
   BEI(IT)=BE1
   DEI(IT)=DEL(IT)
21 CONTINUE
   IBP2=I8P1
   Y2=Y1
   DO 25 IT=1.25
   T12=0.5D0+(TH1+TH2)
   P12=0.5D0+(PS1+PS2)
   B12=0.5D0+(BE1+BE2)
   SINT12=DSIN(T12)
   COST12=DCOS(T12)
   SINP12=DSIN(P12)
   COSP12=DCOS(P12)
   SINB12=DS[N(812)
   COSB12=DCOS(812)
   N1=0.500*(N11+N12)
   N2=0.5D0+(N21+N22)
   N3=0.500*(N31+N32)
   CC1=N3*COST12*COSP12-N1*COST12*S1NP12
   CC 2=N1 *SI NT12-N2*COST12*COSP12
   CC3=(N3+SINT12-N2+COST12+SINP12)+DZ+CC1+X1+CC2+Y1
   Y20=Y2
   [BP=[BP2
   X20=X2
   CALL SOL VBP(X2,Y2,CC1,CC2,CC3,A2,B2,C2,IT2,X20,Y20)
   CALL CKBDYP(X2,Y2,X8,Y8,18P2)
   IF(IBP.NE.IBP2) CALL BOYFIT(A2.B2.C2.X8.Y8.IBP2.IT2)
   CALL NORMAL(X2.Y2.ZE+DZ.A2.B2.C2.N12.N22.N32.IT2.IBP2)
   SINT2=DSIN(TH2)
   CDST2=DCOS(TH2)
   SINP2=DSIN(PS2)
   COSP2=DCOS(PS2)
   DEL(1) =DARCOS(-N12+SINT2+COSP2+N22+COST2-N32+SINT2+
  *SINP2)
   IF(N32,LT.0.00) DEL(1)=6.28318530700-DEL(1)
   DEL(2) =DEL(1)-1.570796327D0
```

```
IF(DEL(2).LT.0.D0) DEL(2)=6.283185307D0+DEL(2)
  DEL(3)=DEL(1)+1.570796327D0
   IF(DEL(3).GT.6.283185307D0)
  *DEL(3)=DEL(3)-6.283185307D0
  DO 23 J=1.3
   T21(J)=0.500*(TH2+TH((J))
  P2I(J)=0.5D0*(PS2+PI1(J))
  B2I(J)=0.500*(BE2+BEI(J))
  D2I(J)=0.5D0+(DEL(J)+DEI(J))
   D2I(J)=D2I(J)-3.141592654D0
   IF(D2I(J).LT.0.DQ) D2I(J)=6.283185307D0+D2I(J)
   SINT2I(J)=DSIN(T2I(J))
  COST21(J)=DCOS(T21(J))
   SINP2[(J)=DSIN(P2I(J))
   COSP2I(J)=DCOS(P2I(J))
   SINB2I(J)=DSIN(B2I(J))
  COSB2I(J)=DCOS(B2I(J))
   SIND 21 ( J) =DSI N(D21 ( J) )
  CDSD2I(J) = DCDS(D2I(J))
   F1=SINB2I(J)+COSD2I(J)
   F2=SINB2((J) #SIND21(J)
   F3=C0S82[(J) +C0ST2[(J)-F1 +SINT2[(J)
  DL(J)=DZ/(F3+COSP2[(J)-F2+SINP2!(J))
  DX(J)=SINT2I(J)*COSB2I(J)*F1*COST2I(J)
   DY( J)=F3*SINP2[(J)+F2*C0SP2[(J)
   (L) \perp (d) \times (d) \times (d) \times (d)
   YI(J)=Y2-DY(J) *DL(J)
  CALL GETPT(XI(J).YI(J).PP(1.J))
  RAD=D SQRT(G +PP(1.J)/PP(2.J))/PP(3.J)
   IF((RAD.GE.O.DO).AND.(RAD.LE.1.DO)) GO TO 22
   WRITE(6.2)I,J.P1.R1.Q1.TH1.PS1.BE1.P2.R2.Q2.TH2.PS2.
  *BE 2.P20.R20.Q20.T20.PSC.DEL(1).DEL(2).DEL(3).N11.N21.
  *N31.N12.N22.N32.N1.N2.N3.DL(J).DX(J).DY(J).DEI(J).
  .(l)!!!q.(l}!HT.(l,5)9q.(l,4)9q.(l,6)9q.(l,5)9q.(l,1)
  *8EI(J)
 2 FORNAT('1 FAILED IN BODY AT I='.I3.5X.'J='.I3//
  *1P6E14.5/6E14.5/5E14.5/3E14.5/9E14.5/4E14.5/8E14.5)
   STOP
22 CONTINUE
   CALL DELTAF(J,DEL(J),DE1(J))
   IF(DABS(DEI(J)).LE.1.0-8) DEI(J)=0.D0
   CALL GETDER(XI(J).YI(J).DER)
   PI(J)=PP(1.J)
   {L,4}99=(L)IHT
   P[1(J)=PP(5.J)
   BEI(J) = DARSIN(DSQRT(G*PP(1.J)/PP(2.J))/PP(3.J))
   T2I(J)=0.5D0+(TH2+THI(J))
   P2I(J)=0.5D0*(P52+PII(J))
  B2I(J) =0.5D0*(BE2+BE1(J))
  D2I(J)=0.5D0+(DEL(J)+DE((J))
```

```
D2I(J)=D2I(J)-3.141592654D0
  IF(D2I(J).LT.0.D0)
                      D2I(J)=6.283185307D0+D2I(J)
  SINTZI(J)=DSIN(TZI(J))
  COST21(J)=DCGS(T21(J))
  $INP2I(J) =DSIN(P2I(J))
  COSP2[(J)=DCOS(P2[(J))
  SINB2I(J)=DSIN(B2I(J))
  CDS821(J)=DCOS(B21(J))
  SIND2I(J)=DSIN(D2I(J))
  COSD2I(J) =DCOS(D2I(J))
                                              1
  DTDX(J)=DER(1.4)
  DPDX(J)=DER(1.5)
  DTDY(J)=DER(2.4)
  DPDY(J)=DER(2.5)
  F1=COST2I(J) #SIND2I(J)
  #2=SINT2[(J) #5IND2I(J)
  F3=SINB2I(J) *DL(J)
  F4=COST2I(J) *COSD2I(J)
  DXDN(J)=-F1
  DYDN(J1=F2+SINP2I(J)+CQSP2I(J)+CQSD2I(J)
  DZDN(J)=F2*COSP2I(J)*SINP2I(J)*COSO2I(J)
  F5=X1(J)-X2
  F6=Y1(J)~Y2
  DTDZ(J)=(DTDX(J)+F5+DTDY(J)+F6)/DZ
  DPDZ(J)=(DPDX(J)*F5+DPDY(J)*F6)/DZ
  AL(1,J)=COSB2[(J)/(SINB2[(J)*PP(2,J)*PP(3,J)**2)
  AL(2.1)=COSD2I(J)-F3+SIND2I(J)+DZDN(J)/DZ
  AL(3-J)=F1+F3+F4+DZDN(J)/DZ
  CR(J)=F3*{SIND21(J)*(DTDX(J)*DTDY(J)*DYDY(J)*DYDY(J)}
  *DTDZ(J)*DZDN(J))~F4*{DPOX(J)*DXDN(J)*DZDN(J)*PDN(J)
  *DPDZ(J)*DZON(J)))+AL(1.J)*PI(J)+AL(2.J)*THI(J)+AL(3.J)
  (L)!!9**
23 CONTINUE
   A1=AL(2.1) +AL(1.2) ~AL(1.1) +AL(2.2)
  B1=AL(3.1) +AL(1.2) -AL(1.1) +AL(3.2)
   C1=CR(1) *AL(1.2)-AL(1.1) *CR(2)
   AM(2.1)=TH2
   AM(3.1)=PS2
  CALL NEWRAP(AM(2.1).AM(3.1).A1.B1.C1.N12.N22.N32)
   A1=AL(2.2)*AL(1.3)-AL(1.2)*AL(2.3)
   B1=AL(3,2) *AL(1,3)-AL(1,2) *AL(3,3)
   C1=CR(2) *AL(1.3)-AL(1.2) *CR(3)
   AM(2.2)=TH2
   AN(3.2)=PS2
   CALL NEWRAP(AM(2.2).AM(3.2).A1.B1.C1.N12.N22.N32)
   A1=AL(2.3) +AL(1.1) -AL(1.3) +AL(2.1)
   B1=AL(3,3) *AL(1,1)-AL(1,3) *AL(3,1)
   C1=CR(3)*AL(1.1)-AL(1.3)*CR(1)
   2HT=(E.S)MA
   AM(3.3)=PS2
```

```
CALL NEWRAP(AM(2.3).AN(3.3).A1.B1.C1.N12.N22.N32)
   AM(1,1)=(CR(1)-AL(2,1)+AM(2,1)-AL(3,1)+AM(3,1))/AL(1,1)
   AM(1,2)=(CR(2)-AL(2,2)+AM(2,2)-AL(3,2)+AM(3,2)]/AL(1,2)
   AM(1.3) = (CR(3) - AL(2.3) + AM(2.3) - AL(3.3) + AM(3.3) / AL(1.3)
    P2=0.500*(AM(1.1)+AM(1.3))
    TH2=0.5D0*(AM(2.1)+AM(2.3))
   PS2=0.5D0*(AN(3.1)+AN(3.3))
    T2=TTOD*(P2/PTOD(I))*+GN1G
   R2=P2/(R0+T2)
   02=DSQRT(2.D0+GGM1+R0+(TTOD-T2))
    IF(IT.EQ.1) GO TO 24
    IF(DABS((P2-P20)/P2).LE.1.0-7) GO TO 26
    IF([T.EQ.25) GO TO 25
24 CONTINUE
   P20=P2
   R20=R2
    020=02
    T20=TH2
    PSO=PS2
   BE2=DARSIN(DSQRT(G*P2/R2)/Q2)
25 CONTINUE
    IF(DABS((P2-P20)/P2).LE.1.D-5)
                                    60 TO 26
    WRITE(6.1)I.ZE.DZ.X1.Y1.P1.TH1.PS1.X2.Y2.P2.TH2.PS2.
   *P20.T20.PS0
    IF(DABS((P2-P20)/P2).GT.1.D-4)
                                      STOP
 26 CONTINUE
    x = \{1\} | x \ge x \ge x
    YN( [ )=Y2
    PN([]=P2
    RN(I)=R2
    QN(1)=Q2
    TN([]=TH2
    PSN( [ ) =PS2
    RETURN
    END
```

```
SUBROUTINE CARDIN
   DIMENSION A(20)
 1 FORMAT(20A4)
 2 FORMAT(5X,20A4)
 3 FORMAT( 11 +,38X, 1 INPUT CARDS 1)
 4 FORMAT( *0 *.4 X.9( *0 *) .10( *1 *) .10( *2 *) .10( *3 * ) .10( *4 *) .
  *10("5"),10("6"),10("7"),"8"/5X,8("1234567890")/)
   IP=50
   WR [ TE ( 6.3)
   WRITE(6.4)
20 CONTINUE
   READ(5.1.END=99)A
   IF([P.NE.0) GO TO 21
   WRITE(6.4)
   WRITE(6.3)
   WRITE(6.4)
   IP=50
21 CONTINUE
   WRITE(6,2)A
   WRITE(8.1)A
   IP=IP-1
   GD TO 20
99 CONTINUE
   REWIND 8
   WRITE(6.4)
   RE TURN
   END '
```

```
SUBROUTINE CUT (ZB)
   COMMON /BCUT/X8(50) YB(50)
   COMMON /GEOM/ZC(50) .XC(50.50) .YC(50.50) .NS .NP
   REAL *4 A(3.3)
   Z=ZB
   DO 21 I=2.NS
   IF(ZB.LE.ZC(1)) GO TO 22
21 CONTINUE
   I = NS - 1
22 CONTINUE
   IF(I.EQ.NS)
                 I = NS - 1
   1P=I+1
   I M=I-1
   Z0=ZC(IM)
   Z1=ZC(I)
   Z2=ZC(IP)
   Z10=1.9/(Z1-Z0)
   Z20= 1.0/(Z2-Z0)
   Z21=1.0/(Z2-Z1)
   ZP1=Z0+Z1
   A(3.1)=Z21+(Z10-Z20)
   A(3,2)=-Z21+Z10
   A(3.3) = Z21 * Z20
   A(2,1) = -Z10 - ZP1 + A(3,1)
   A(2.2) = Z10-ZP1*A(3.2)
   =(E.S)A
             -ZP1 *A(3.3)
   A(1.1)=-Z0+(A(2.1)+A(3.1)+Z0)+1.0
   A(1.2)=-Z0+(A(2.2)+A(3.2)+Z0)
   A(1.3) = -20*(A(2.3)+A(3.3)*20)
   DO 23 J=1.NP
   B=A(1.1)+XC(J.IM)+A(1.2)+XC(J.I)+A(1.3)+XC(J.IP)
   C=A(2.1)*XC(J.IM)*A(2.2)*XC(J.I)*A(2.3)*XC(J.IP)
   D=A(3,1)*xC(J,IM)+A(3,2)*xC(J,I)+A(3,3)*xC(J,IP)
   XB(J)=8+(C+D+Z)+Z
   B=A(1.1) +YC(J.IM)+A(1.2) +YC(J.I)+A(1.3)+YC(J.IP)
   C=A(2,1)*YC(J,IM)*A(2,2)*YC(J,I)*A(2,3)*YC(J,IP)
   (91 eL)2Y*(EeE)A+(1,L)2Y*(SeE)A+(M1eL)2Y*(1,E)A=C
   YB{ J} =B+ { C+D +Z } +Z
23 CONTINUE
                                             >--
   RETURN
   END
```

```
SUBROUTINE DELTAF (J.DEL.DELI)
   IMPLICIT REAL+8(A-H+G-Z)
  COMMON /FLOBDY/DUMMY(14),SINTI(4),COST 1(4),SINPI(4),
  *COSPI(4).SINBI(4).CGSBI(4)
  A=SINTI(J) +COSPI(J) +SINBI(J)
  B=SINPI(J) +SINBI(J)
  C=-0.5D0*CDSTI(J)*CDSPI(J)*(SINBI(J)+CDSBI(J))
   SIND=DSIN(DEL)
  COSD=DCOS(DEL)
  DELI =DEL
   A 58 S=A ++2+B ++2
  RAD=ASBS-C**2
   IF(RAD.LT.O.DO) RETURN
  RAD=DSQRT(RAD)/ASBS
   SINI=8 +C/ASBS
   SINII=SINI+A*RAD
   SINI2=SINI-A#RAD
   IF(DABS(SIND-SINI2).LT.DABS(SIND-SINI1))
                                              GD TD 21
   SINI=SINI1
                            GO TO 22
   IF(DABS(SINI).LE.1.DO)
21 CONTINUE
   SINI=SINI2
   IF(DABS(SINI).GT.1.DO)
                            SINI=SINI1
   IF(DABS(SINI).GT.1.DO)
                            RETURN
22 CONTINUE
   COSI = A +C /ASBS
   COSI 1=COSI+B*RAD
   COSI 2=COSI-B*RAD
   IF(DABS(COSD-COS12).LT.DABS(COSD-COS11)) GO TO 23
   COST=COST1
   IF(DABS(COSI).LE.1.DO) GO TO 24
23 CONTINUE
   COSI=COSI2
   IF(DABS(COSI).GT.1.DO) COS[=COSI1
   IF(DABS(COSI).GT.1.DO) RETURN
24 CONTINUE
   DELI=DATAN2(SINI+COSI)
   IF(DELI.LT.0.00) DELI=6.283185307D0+DELI
   RETURN
   END
```

```
SUBROUTINE DISTIDELS)
   COMMON /GAS/G,RO.GM1.GM1H.GM1G.GGM1.GP1.GPGM
   CDMMON/VALUE/ZE+X(1000)+Y(1000)+P(1000)+RHO(1000) +
  *Q(1000),THETA(1000),PSI(1000),N
   INTEGER #2 NE(8.1000)
   COMMON /NEAR/NE-DMIN
   DMIN=1.E10
   QMIN=1.E10
   O.O=X AMA
   DO 22 I=1.N
   A=P(I)/RHO(I)
   IF(A.GT.AMAX) AMAX=A
   IF(Q(I).LT.OMIN) QMIN=Q(I)
   DD 21 J=1.8
   K=NE(J.[)
   D=(X(1)-X(K)) ++2+(Y(1)-Y(K))++2
   IF (D.LT.DMIN) DMIN=D
21 CONTINUE
22 CONTINUE
   AMAX=SQRT(G +AMAX)
   DELS=QMIN*SQRT(DMIN)/AMAX
   DELS=SQRT(DMIN*ABS((QMIN/AMAX)**2-1.0))
   RETURN
   END
```

```
SUBROUTINE FIELD(I)
  [MPLICIT REAL +8(A-H, 0-Z)
  REAL+4 ZD.XN(1000).YN(1000).PN(1000).RN(1000).GN(1000).
 *PSN(1000).ZE.X{1000}.Y(1000).P(1000).RHD(1000) .
 *TN(1000).PSI(1000).Q(1000).THETA(1000)
  COMMON /NVALU/ZD.XN.YN.PN.RN.QN.TN.PSN
  COMMON /VALUE/ZE.X.Y.P.RHO.Q.THETA.PSI.N
  CDMMON /DGAS/DZ.G.RO.GM1.GM1H.GM1G.GGM1.GP1.GPGM
  COMMON/DSTAG/PTOD(1000).TTOD.ATOD
  COMMON/IDEBUG/IDBUG(80)
  COMMON /POINT/X1.Y1.P1.R1.Q1.T1.TH1.PS1.BE1.X2.Y2.P2.
 *R2,Q2,T2.TH2,PS2,BE2,P20,T20,PS0,DEL(4),PI(4),THI(4),
 *P11(4).BEI(4).X((4).YI(4).DEI(4).DX(4).DY(4).DL(4).
 *PP(5,4),T12,P12,B12,T21(4),P21(4),B21(4),D21(4)
  COMMON /FLDBDY/SINT12.COST12.SINP12.COSP12.SINB12.
 *COSB12.SIND2I(4).COSD2[{4}.SINT2I{4}.COST2I[4].
 *SINP21(4).COSP21(4).SIN821(4).COS821(4).DXDN(4).
 *DYDN(4)*DZDN(4)*DTDX(4)*DTDY(4)*DTDZ(4)*DPDX(4)*
 *DPDY(4).DPDZ(4).DER(2.5).AL(3.4).CR(4).AM(3.3).CN(3.4)
1 FORMAT('O FAILED IN FIELD AT POINT'.15.5%."Z1=".
 +1PE12.5.5X.*DZ=*.E12.5//5X.*X1=*.E12.5.5X.*Y1=*.E12.5.
 *5x, 'P] = '.E12.5.5X, 'T1='.E12.5.5X, 'PS1='.E12.5/5X, 'X2='
 *.E12.5.5X, 'Y2='.E12.5.5X, 'P2='.E12.5.5X, 'T2='.E12.5.5X
 *. 'PS2='.E12.5/45X+'P20='.E12.5.4X+'T20='.E12.5.4X+
 **PS20='.E12.5//}
  x1 \Rightarrow x(1)
  Y1=Y([]
  DEL(1)=0.D0
  If(X1.NE.0.D0.OR.Y1.NE.0.D0) DEL(1)=DATAN2(Y1.X1)
                        DEL(1)=6.283185307D0+DEL(1)
  [F(DEL(1).LT.O.DO)
  DEI(1)=DEL(1)
  DO 20 IT=2.4
  DEL(IT)=DEL(IT-1)+1.570796327D0
  IF(DEL(IT).GE.6.283185307D0)
  *DEL(IT)=DEL(IT)-6.283185307D0
  DEI(IT)=DEL(IT)
20 CONTINUE
  P1=P(I)
  R1 = RHO(1)
  0.1 = 0(1)
   TH1=THETA(I)
  PS1=PSI(I)
   T1=P1/{R0*R1}
  P2=P1
  R2=R1
  Q2 = Q1
   TH2=TH1
   P52=PS1
   T2=T1
   BE1=DARSIN(DSQRT(G*P1/R1)/Q1)
```

```
BE 2=BE1
  DO 21 IT=1.4
   THI(IT)=TH1
   PII(IT)=PS1
   BEI(IT)=BE1
21 CONTINUE
   DO 26 [T=1.25
   T12=0.5D0*(TH1+TH2)
   P12=0.5D0+(PS1+PS2)
  812=0.500*(BE1+BE2)
   SINT12=OSIN(T12)
  COST12=DCOS(T12)
   S[NP12=DSIN(P12)
  COSP12=DCOS(P12)
   SINB12=DSIN(812)
  COSB12=DCOS(B12)
   X2=X1+SINT12+DZ/ICOST12+COSP121
   Y2=Y1+SINP12+0Z/COSP12
  DO 22 J=1,4
   T2I(J) = 0.500*(TH2+THI(J))
  P21(J)=0.5D0+(PS2+P(1(J))
  B2I(J)=0.500+(BE2+BEI(J))
  D2I(J)=0.5D0+(DEL(J)+DEI(J))
   SINTEC(U) SINCTEL(J))
  COST2I(J)=DCCS(T2I(J))
   SINP2I(J)=DSIN(P2({J}))
  COSP2I(J) = DCOS(P2I(J))
   SINB2I(J)=DSIN(B2I(J))
  CDSB2[(J)=DCOS(B2[(J))
   SIND2I(J)=DSIN(D2I(J))
  COSD2I\{J\}=DCOS(D2I\{J\})
  F1=$[NB2[(J) +C0SD2[(J)
  F2=SINB2I(J) *SIND2I(J)
  F3=COS821(J)+COST21(J)-F1+SINT21(J)
  DL(J)=DZ/(F3+COSP2[(J)-F2+S[NP2[(J))
  DX(J)=SINT2I(J)+COSB2I(J)+F1+COST2I(J)
  DY(J)=F3+SINP2I(J)+F2+C0SP2I(J)
   XI(J) = X2 - DX(J) *DL(J)
   YI(J)=Y2-DY(J)*DL(J)
  CALL GETPT(XI(J),YI(J),PP(1.J))
  IF(DABS(PP(4.J)).LT.1.D-81 PP(4.J)=0.00
   IF(DABS(PP(5,J)).LT.1.D-8)
                                PP(5.J)=0.00
  CALL DELTAF(J.DEL(J).DEI(J))
   IF(DABS(DEI(J)).LE.1.0-8) DEI(J)=0.D0
  CALL GETDER(XI(J).YI(J).DER)
  (L, 1)99 = (L)19
   (L. 4) 99=(L) IHT
  PII(J)=PP(5.J)
  BET(J)=DARSIN(DSQRT(G*PP(1.J)/PP(2.J))/PP(3.J))
  T2I(J) = 0.500 + (TH2 + THI(J))
```

```
P21(J)=0.5D0*(PS2+PII(J))
       821(J)=0.500*(BE2+8E1(J))
       D2I(J)=0.5D0+(DEL(J)+DEI(J))
       SINT21(J) =DSIN(T21(J))
       CDST2[(J)=DCDS(T21(J))
       SINP2I(J)=DSIN(P2I(J))
       COSP2I(J) = OCOS(P2I(J))
       SINB2I(J)=DSIN(B2[(J))
       COSB 21 ( J) = DCGS ( B2 ( ( J) )
       SIND2I(J)=DSIN(D2I(J))
       COSD2I(J)=DCOS(D2I(J))
       DTDX(J)=DER(1,4)
       DPD x{ J) = DER(1.5)
       DTDY( J) = DER(2.4)
       DPDY(J)=DER(2.5)
       F1=COST2I(J) #SIND2I(J)
       F2=SINT2I(J) #SIND2I(J)
       F3=SINB21(J) +DL(J)
       F4=C0ST2I(J) *C0SD2I(J)
       DXDN(J) = -F1
       DYDN( J) =F2 +S I NP2 I ( J) + COSP2 I ( J) + COS D2 I ( J)
       DZON(J)=F2*COSP2I(J)-S1NP2I(J)*COSD2I(J)
       F5=XI(J)-X2
       F6=Y1(J)-Y2
       DTDZ(J)=(DTDX(J)*F5+DTDY(J)*F6)/DZ
       OPD 2(J) = (OPD x(J) *F5+DPD y(J) *F6)/DZ
       AL(1.J)=COSB2I(J)/(SINB2I(J)*PP(2.J)*PP(3.J)**2)
       AL(2.J)=COSD2I(J)+F3+SIND2I(J)+DZDN(J)/DZ
        AL(3.J)=F1+F3+F4+D2DN(J)/DZ
       CR(J)=F3*(SIND2I(J)*(DTDX(J)*DXDA(J)*DYDJ)*(J)*DYDJ)+
     +CTDTDZ(J)+CZQ+(L))-F4+(DPOX(L)+CXQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L)+CZQ+(L
     *DPDZ(J)*DZDN(J)))+AL{1.J)*PI(J)+AL(2.J)*THI(J)+AL(2.J)
     **PII(J)
22 CONTINUE
       DD 24 M=1,4
       L=N
       DO 23 J=1.3
        AM( J.1 )=AL(1.L)
        AM( J.2) = AL(2.L)
        AM(J,3)=AL(3,L)
       CM(J.M)=CR(L)
       L=L+1
        IF(L.GT.4) L=1
23 CONTINUE
       CALL SIMQ(AM.CM(1.M).3.1)
24 CONTINUE
       P2 = 0.2500 + (CM(1.1) + CM(1.2) + CM(1.3) + CM(1.4))
        TH2=0.25D0+(CM(2.1)+CM(2.2)+CM(2.3)+CM(2.4))
        PS2=0.2500*(CM(3.1)+CM(3.2)+CM(3.3)+CM(3.4))
        T2=TTOD*(P2/PTOD(1)) **GM1G
```

```
R2=P2/(R0+T2)
  Q2=DSQRT(2.00+GGM1+RC+(TTCD-T2))
   1F(IT.EQ.1) GO TO 25
   IF(DABS((P2-P20)/P2).LE.1.D-7) GO TO 27
   IF([T.EQ. 25) GO TO 26
25 CONTINUE
  P20=P2
  R20=R2
  Q20=Q2
   T20=TH2
  PS0=PS2
  BE2=DARSIN(DSQRT(G*P2/R2)/Q2)
26 CONTINUE
  IF(DABS((P2-P20)/P2).LE.1.D-5) GO TO 27
   WRITE(6.1)[.ZE.0Z.X1.Y1.P1.TH1.PS1.X2.Y2.P2.TH2.PS2.
  *P20.T20.P50
  IF(DABS((P2-P20)/P2).GT.1.D-4) STOP
27 CONTINUE
   XN[I]=X2
   SY=(1)NY
  PN(I)=P2
  RN(I)=R2
  QN(I)=Q2
   TN(1)=TH2
  PSN(I)=PS2
  RETURN
  END
```

AEDC-TR-78-68

```
SUBROUTINE FIND(I .L1 .L3 .NE)
   INTEGER#2 NE(1)
  REAL*4 DIST(3)
  COMMON/VALUE/ZE.X(1000).Y(1000)
  L2=L1+L3
   J=0
  DO 22 L=L1.L2
  D=(X(I)-X(L)) *#2+(Y(I)-Y(L)) *#2
   IF(J.EQ.3) GO TO 21
   1+L=L
   NE(J)=L
  DEST(J)=0
   EF(J.NE.3) GO TO 22
   CALL SORT(DIST.NE.3)
   GO TO 22
21 CONTINUE
 + (F(0.GE.DIST(3)) GD TO 22
   DIST(3)=D
  NE(B)≡L
   CALL SORT(DIST.NE.3)
22 CONTINUE
   RETURN
   END
```

SUBROUTINE FINDBP(X1.Y1.X8.Y8.IRGINT) COMMON /GEOM/ZC(50),XC(50,50).YC(50.50).NS.NP DIMENSION XB(50).YB(50) 20 CONTINUE IPOINT=1 DMIN=(X1-XB(1))++2+(Y1-YB(1))++2DO 21 J=2.NP D=(X1-XB(J))++2+(Y1-YB(J))++2IF(D.GE.DMIN) GD TO 21 L=TM1091 DMI N=D 21 CONTINUE **RETURN** ENTRY CKBDYP(X1.Y1.X8.Y8.IPOINT) DMIN=(X1-X8(J)) ++2+(Y1+Y8(J)) ++2 」≃」-1 IF(J.EQ.O) J=NP D=(X1-XB(J)) ++2+(Y1-YB(J)) ++2 IF (D.LT.DMIN) GO TO 20 J=IPOINT+1 IF(J.GT.NP) J≖1 D=(X1-XB(J)) **2+(Y1-YB(J)) **2 IF(D.LT.DMIN) GO TO 20 RETURN END

```
SUBROUTINE FIT(I)
  CDMMDN/VALUE/ZE.X(1000).Y(1000).P(1000).RHU(1000) .
  #Q(1000).THETA(1000).PSI(1000).N
   INTEGER#2 NE(8.1000)
   COMMON /NEAR /NE
   REAL+8 R.B(12.12).C(12.5).VAL(5).DER(2.5).DX.DY.FAC
   DO 22 J=1.12
   1F(J.GT.9) GO TO 21
   B(1.J)=1.D0
   K=I
   IF(J.NE.1) K=NE(J-1.1)
   B(2.J)=X(K)
   8(3,J)=Y(K)
   GO TO 22
21 CONTINUE
   8(1.J)=0.D0
 . B(2.J)=0.D0
   B(3.J)=0.D0
22 CONTINUE
   DO 24 JJ=4,11
   J=13-JJ
   KL=J-1
   K1=I
   IF(J.NE.1) K1=NE(KL.I)
   DO 23 K=1.KL
   K2=I
   IF(K.NE.1) K2=NE(K-1.1)
   R=(X(K1)-X(K2))++2+(Y(K1)-Y(K2))++2
   B(JJ_*K)=R*DLOG(R)
23 CONTINUE
   0G.0=(L.LL)B
24 CONTINUE
   B(12.1)=0.D0
   DO 26 J=1.11
   K=13-J
   KL=K-1
   DO 25 L=1.KL
   B(K.13-L)=8(L.J)
25 CONTINUE
26 CONTINUE
   DO 29 J=1.12
   IF(J.GT.3) GO TO 28
   DO 27 K=1.5
   C(J.K)=0.D0
27 CONTINUE
   GD TO 29
28 CONTINUE
   KL=13-J
   K=I
   IF(KL.NE.1) K=NE(KL-1.1)
```

```
C(J.1)=P(K)
   C(J+2)=RHO(K)
   C(J,3)=Q(K)
   C(J,4)=THETA(K)
   C(J,5)=PSI(K)
29 CONTINUE
   CALL SIMQ(8.C.12.5)
   RETURN
   ENTRY GETPT(X1.Y1.YAL)
   DO 30 J=1.5
   VAL(J)=C(12,J)+C(11,J)+X1+C(10,J)+Y1
30 CONTINUE
   DO 32 J=1.9
   K=[
   [F(J.NE.1) K=NE(J-1.1)
   R={X1-X(K)} **2+{Y1-Y(K)} **2
   IF(R.EQ.O.DO) GO TO 32
   DO 31 L=1.5
   VAL(L) = VAL(L) + C(J_*L) *R*DLGG(R)
31 CONTINUE
32 CONTINUE
   RETURN
   ENTRY GETDER(X1.X2.DER)
   DO 33 J=1.5
   DER(1.J)=C(11.J)
   DER(2.J) =C(10.J)
33 CONTINUE
   DO 35 J=1,9
   K≖I
   IF(J.NE.1) K=NE(J-1.1)
   DX=X1-X(K)
   DY=Y1-Y(K)
   R=DX**2+DY**2
   IF(R.EQ.O.DO) GO TO 35
   DO 34 L=1.5
   FAC=2.D0+C(J.L)+(1.D0+DLOG(R))
   DER(1.L)=DER(1.L)+FAC+DX
   DER(2.L)=DER(2.L)+FAC+DY
34 CONTINUE
35 CONTINUE
   RETURN
   END
```

END

```
SUBROUTINE IDENT(I)
  IF(1.EQ.2) GO TO 21
  CALL CALCMP(15.0.2.0.10.0)
  CALL SYMBOL(0.5.7.5.0.84. FOLLOWING PLOTS FOR .0.0.19)
  CALL SYMBOL(1.2.5.5.0.98. W. C. ARMSTRONG .0.0.15)
  CALL SYMBOL(5.5.3.5.0.84. CSB-EA0'.0.0.7)
  CALL CLASS(1.3.0.0)
  CALL CALCMP(0.5.0.5.0.3)
  RETURN
21 CONTINUE
  CALL CALCMP(0.0.0.0.0.3)
  CALL CLASS(4.3.0.0)
  CALL SYMBOL(.08,7.5.0.84, PRECEEDING PLOTS FOR .0..20)
  CALL SYMBUL(1.2.5.5.0.98, W. C. ARMSTRONG', 0.0.15)
  CALL SYMBOL(5.5.3.5.0.84.1CS8-EAD1.0.0.7)
  CALL CALCMP(0.0.0.0.9999.21
  RETURN
```

```
SUBROUTINE INGEOM
      COMMON /TITLE/HEAD(20)
      COMMON /GEOM/ZC(50).XC(50.50).YC(50.50).NS.NP
      COMMON/IDEBUG/IDBUG(80)
      COMMON/VALUE/X(50.50).Y(50.50).S(50).IT(50).IV(50)
    1 FORMAT( 11 . 10 X . 20 A4 / / 20 X . 'GEOMETRY [NPUT' . 10 X .
     *'NO. OF STATIONS =',13/)
                   Z = 1.1 PE13.5.5X.1 IV = 1.13.5X.1 IT = 1.12//
    2 FORMAT( 'O
     *8X. 'X' .14X. 'Y'/)
    3 FORMAT(1P2E15.5)
    4 FORNAT('1'+10X+20A4//20X+'CONVERTED GEOMETRY'//)
    5 FORMAT(215.E10.0)
    6 FORMAT(8E10.0)
C
          IV= NO. OF POINTS AT THIS STATION
C
          IT= 1 - ALL POINTS GIVEN IN RECTANGULAR COORDINATES
C
               2 - ALL POINTS GIVEN IN POLAR COORDINATES
C
               3 - ONE POINT GIVEN IN POLAR COORDINATES
      READ(8.5)NS
      IF(IDBUG( 1).NE.0)
     *WRITE(6.1)HEAD.NS
      DO 21 I=1.NS
      READ(8.5) IV(1). IT(1). ZC(1)
      IF(IDBUG( 1).NE.0)
     *WRITE(6.2)ZC(I).IV(I).IT(I)
      N=IV(I)
      [F(IT(I).EQ.3) N=1
      READ(8,6)(X(J.I),Y(J.I),J=1,N)
      IF(108UG( 1).NE.0)
     *WR[TE(6.3)(X(J,I],Y(J,I),J=1.N)
   21 CONTINUE
      DD 26 I=1.NS
      IF(IDBUG( 2).NE.0)
     +WRITE(6.4)HEAD
      [F(IOBUG( 2),NE.0)
     *WRITE(6,2)ZC(I), [V(I), IT([)
      N=IV(I)
      IF(IT(I).EQ.1) GO TO 25
      IF(IT(I).Eq.2)
                       GO TO 23
      N\0.0360.0/N
      Y(1.1)=0.0
      DO 22 J=2.N
      X(J-1)=X(1-1)
      Y(J,[]=(J-L)+DT
   22 CONTINUE
   23 CONTINUE
      DD 24 J=1.N
      XX=X(J.I) *COS(0.01745329*Y(J.I))
      Y(J.I)=X(J.I) #SIN(0.01745329#Y(J.I))
      X(J_*I)=XX
   24 CONTINUE
```

END

```
25 CONTINUE
   IF(IDBUG( 2).NE.0)
  *WRITE(6.3)(X(J.I),Y(J.I),J=1.N)
26 CONTINUE
   NP=IV(1)
   DO 27 I=2.NS
   IF(NP.GE.IV([]) GO TO 27
   NP=IV(I)
27 CONTINUE
   NPM=NP-1
   FAC=1.0/NRM
   DO 33 I=1.NS
   N=[V(I)
   S(1)=0.0
   DO 28 J=2.N
   S(J)=S(J-1)+SQRT((X(J-1)-X(J-1-1))+*2+
  4(Y(J,I)-Y-(J-I,I))++2)
28 CONTINUE
   DS=S(N) #FAC
   XC(1.1)=X(1.1)
   YC(1.1)=Y(1.1)
  XC(NP_*I)=X(N_*I)
   YC(NP*I)=Y(N*I)
   KL=2
   00 32 J=2,NPM
   SP=DS*(J-1)
   DO 29 K=KL.N
   IF(SP-S(K))31,30,29
29 CONTINUE
   K=N
30 CONTINUE
   XC(J+I)=X(K+I)
   YC(J.[]=Y(K.[)
   KL=K
   GO TO 32
31 CONTINUE
   RAT=(SP-S(K-1))/(S(K)-S(K-1))
   XC(J_*I)=X(K-I_*I)+(X(K_*I)-X(K+I_*I))*RAT
   YC(J,I)=Y(K-1,I)+(Y(K,I)-Y(K-1,I))*RAT
   KL=K
32 CONTINUE
33 CONTINUE
   RE TURN
```

```
SUBROUTINE INPUT
      COMMON /TITLE/HEAD(20)
      COMMON/VALUE/ZE.X(1000).Y(1000).P(1000).RHD(1000) .
     *Q(1000).THETA(1000).PSI(1000).N
      COMMON /STAG/PTO(1000).TTO.ATOT.ZO.ZMAX.NB(200).
     *NBO(200) .JMAX.JPT.IB.IPLOT.IT11.IT12
      COMMON /GAS/G.RD.GM1.GM1H.GM1G.GGM1.GP1.GPGM
      COMMON/IDEBUG/IDBUG(80)
      INTEGER#2 NB.NBO
      COMMON/NVALU/XR(20), YR(20), PR(20). THR(20). PSR(20).
     #QR(20) .PTR(20)
    1 FORMAT("1"-10X-20A4//20X+"STARTING PLANE INPUT"//5X+
     *'GAMMA ='.F5.3.5X.'PT0 ='.1PE12.5.5X.'TT0 ='.E12.5.
     *5X.'R = '.E12.5)
    2 FORMAT( *O ZO = * *1PE12 *5 *5X * *ZMAX = * *E12 * 5 * 5X * * ITYPE = * *
     #I2.5X,"[MV=",I2,5X,"NPTS=",[5,5X,"NRAYS=",[3,5X,
     **JMAX=*,15,5X,*JPT=*,15/44X,*IPLOT=*,12,4X,*IT11=*,12,
     *5X+*IT12=*+I2+7X+*INEIGH=*+I2//8X+*X*+14X+*Y*+14X+*P*+
     *14X.*Q'.12X.*THETA*.11X.*PSI*.12X.*PTO*//)
    3 FORMAT(1P7E15.5)
    4 FORMAT(7E10.0.15)
    5 FORMAT(2E10.0.1015)
    6 FORMAT( 11 . 10 X . 20 A 4 / / 20 X . • STARTING PLANE VALUES • / / 8 X .
     **X*•14X•*Y*•14X•*P*•13X•*RHO*•13X•*Q*•13X•*THT*•12X•
     *'PSI',12X,'PTO'//(1P8E15.5))
    7 FORMAT( 'O TOO MANY BODY POINTS ')
C
           1 M V=0
                    Q(I)=Q
                                THETA([)=THETA
                                                     PSI(I)=PSI
C
           IMV=1
                    Q(I)=M
                                THETA(I)=THETA
                                                     PSI(I)=PSI
C
           IMV=2
                    Q(I)=W
                                THETA(I)=U
                                                     PS [ ( I )= V
C
                    ONE RAY GIVEN IN POLAR COURDINATES
        [TYPE=0
C
        I TYPE≔1
                     PLANE
                             GIVEN IN POLAR COORDINATES
C
        [TYPE=2
                     PLANE
                             GIVEN IN RECTANGULAR COORDINATES
      READ(8.4)G.PTO.TTC.RO
      WRITE(6.1)HEAD.G.PTO.TTO.RD
      READ(8.5)ZO.ZMAX.ITYPE.INY.NPTS.NRAYS.JMAX.JPT.IPLOT.
     * I T11 . I T12 . I NE (GH
      WRITE(6,2)ZO,ZMAX,[TYPE,IMY,NPTS,NRAYS,JMAX,JPT,IPLOT,
     *IT11.IT12.INEIGH
      N=NP TS
      18=0
      DO 20 I=1.N
      READ(8,4)X(1),Y(1),P(1),Q(1),THETA(1),PSI(1),PTQ(1),NBP
      IF (PTO(I).EQ.O.O)
                           PTO([)=PTO
      IF(IMV.EQ.2) GO TO 19
      THE TA(I) = 0.01745329 * THE TA(I)
           { I }=0.01745329*PSI
                                 (1)
   19 CONTINUE
      TF(NBP.EQ.O) GC TO 20
      19=1R+1
      IE(18.GT.200) GO TO 99
```

```
NB(16)≔I
20 CONTINUE
   IF(IDBUG( 3).NE.0)
  *WRITE(6.3)(X(I).Y(I).P(I).Q(I).THETA(I).PSI(I).
  *PTO(1).I=1.N)
   IF([TYPE.EQ.1)
                    GO TO 24
   IF([TYPE.EQ.2]
                    GO TO 26
   DO 21 I=1.N
   XR(I)=X(I)
   YR([]=Y([)
   PR(I)=P(I)
   QR(I)=Q(I)
   THR(I)=THETA(I)
   PSR(I)=PSI(I)
   PTR(I)=PTO(I)
21 CONTINUE
   18=1
   J=0
   NB[=NB(1)
   DO 23 I=1.N
   J≔J+1
   X(J)=XR(I)
   P(J) = PR(I)
   Q(J)=QR(I)
   THE TA( J) = THR( I)
   PSI(J)=PSR(I Å
   PTO( J) = PTR( 1)*
   IF(I.EQ.1) GO TO 23
   NPTS=3.141593/ARSIN(0.5/FLCAT([-1])+0.5
   DT=360.0/NPTS
   NPTS=NPTS-1
   IF(NBI.EQ.I) NB(18)#J
   DO 22 K=1 NPTS
   J=J+1
   (I) RX = (L)X
   Y(J)=YR(I)+FLOAT(K)+DT
   (1)99 = (1)9
   (1) RD=(L)D
   THETA( J) =THR( I )
   PSI(J)=PSR(I)
   PTO(J)=PTR(I)
   IF(NBI.NE.I) GO TO 22
   IB=IB+1
   IF(18.GT.200) GO TO 99
   N8(1B)=J
22 CONTINUE
23 CONTINUE
   L=M
24 CONTINUE
```

```
DO 25 I=1.N
    ST=SIN(0.01745329*Y(I))
   CT=CDS(0.01745329*Y(1))
   Y(1)=X(1)*ST
   X(I)=X(I)*CT
    TANP=SQRT(TAN(THE-TA(I)) ##2+TAN(PSI(I))##2)
      PSI(I)=ATAN(TANP+ST)
    THETA(1)=ATAN(TANP+CT+COS(PS1(1)))
25 CONTINUE
26 CONTINUE
   A TO T=SQRT (G *RO *TTC)
   GM1=G-1.0
   GM1G=GM1/G
   GP1=G+1.0
   GM1H=0.5*GM1
   GPGM=GP1/GM1
   GGM1 = G/GM1
   XNB=0.0
    0.0=BMY
   DO 261 I=1.18
    J=NB(I )
   XNB=XNB+X(J)
    YNB=YNB+Y(J)
261 CONTINUE
    BI\BNX=BNX
    YNB=YNB/IB
   DO 27 I=1.IB
   J=NB(I)
   RHO(1) = ATAN2(Y(J) - YNB, X(J) - XNB)
    IF(RHO(I).LT.0.0) RHO(I)=6.283185+RHO(I)
   NBO(1)=J
27 CONTINUE
   CALL SORT(RHO.NBO.IB)
   NB(1B+1)=0
   NBD(18+1)=0
   DO 30 I=1.N
    IF(IMV.EQ.1) GO TO 28
   V=Q(I)
   IF(IMV.EQ. 2)
                 V=SQRT(V**2+THETA(1)**2+PS1(1)**2)
    SM=( V/ATOT) **2
   SM=SQRT(SM/(1.0-GM1H+SM))
   IF([MV.EQ.0) GD TO 29
   PS[{1}=ATAN2(PS[{1}).Q(I))
   THETA(1)=ATAN2(THETA(1),Q(1)/CQS(PSI(1)))
   Q[[]=V
   GD TO 29
28 CONTINUE
   Q(1)=SM*ATDT/SQRT(1.0+GM1H*SM**2)
29 CONTINUE
```

```
SM S= SM ++2
   SMFAC=1.0+GM1H+SMS
   T=TTO/SMF AC
  RHO(I)=P(I)/(RO+T)
30 CONTINUE
   IF(IDBUG( 4) . NE . 0)
  *WRITE(6,6)HEAD.(X(I).Y(I).P(I).RHO(I).Q(I).THETA(I).
  *PSI(1),PTQ(1),[=1,N)
   IF((ITYPE.EQ.O).AND.(INEIGH.EQ.O)) INEIGH=1
   IF(INEIGH.EQ.O) CALL NEIGH
   IF(INEIGH.EQ.1) CALL RNEIG
   IF(INEIGH.EQ.2) CALL READNE
   RETURN
99 CONTINUE
   WRITE(6.7)
   STOP
   END
```

```
SUBROUTINE NEIGH
   COMMON/VALUE/ZE,X{1000},Y(1000),P(1000),RHO(1000),
  +Q(1000).THETA(1000).PS[(1000).N
   INTEGER #2 NE(8.1000)
   COMMON /NEAR/NE.DMIN
  COMMON/IDEBUG/IDBUG(80)
  DIMENSION LIST(19) .LONG(19)
  DATA LIST/1.2.8.20.39.64.95.133.177.227.284.347.416.
  *491.573.661.755.856.963/
   DATA LONG/0.5.11.18.24.30.37.43.49.56.62.68.74.81.87.
  *93.100.106.0/
 1 FORMAT('1',20X,'NEIGHBORS',5X,'DMIN =',1PE12.4
  *//6X,'8ASE',9X,'1',9X,'2',9X,'3',9X,'4',
  *9X.'5'.9X.'6'.9X.'7'.9X.'8'//)
 2 FORMAT(9[10]
  DIMENSION DXM(8)
  DMIN=1.E10
  DO 23 I=1.N
   IC=0
  DD 22 J= 1.N
   IF(1.EQ.J) GO TO 22
  2++((L)Y-(1)Y)+2++((L)X-(1)X)=0
   JF(IC.EQ.8) GO TO 21
   IC=IC+1
   NE(IC+[)=J
  DXM(IC)=D
   IF(IC.EQ.8) CALL SORT(DXM.NE(1.1).8)
   GD TO 22
21 CONTINUE
   IF(D.GE.DXM(8)) GO TO 22
   L= (1,8)3K
   D \times M(8) = D
   CALL SURT(DXM.NE(1.1).8)
22 CONTINUE
   IF(DXM(1).LT.DMIN) DM[N=DXM(1)
23 CONTINUE
   60 TO 29
   ENTRY RNEIG
   J=1
   DO 28 [=1.N
   IF(1.GE.LIST(J+1))
   IF(J.NE.1) GO TO 25
   DO 24 K=1.6
   NE(K.1)=K+1
24 CONTINUE
   NE(7.1)=11
   NE(8,1)=17
   GO TO 28
25 CONTINUE .
   LL=I-1
```

```
IF(LL.LT.L[ST(J)) LL=LIST(J+1)-1
  LH=1+1
   [F(LH.GE.LIST(J+1)) LH=LIST(J)
  NE(1.1)=LL
  NE { 2 . 1 }=LH
   IF(J.NE.2) GO TO 26
  LL=LL-1
   IF(LL.LT.LIST(J)) LL=LIST(J+1)-1
  LH=LH+1
   IF(LH.GE.LIST(J+1)) LH=LIST(J)
   NE(3.1)=LL
   NE{4.1}=1 .
   NE(5.1)=LH
   K=J+1
   GO TO 27
26 CONTINUE
   CALL FIND(I.LIST(J-1).LONG(J-1).NE(3.1))
   K=J+1
   TF(N.LT.LIST(K)) K=J-2
27 CONTINUE
   CALL FIND(I.LIST(K).LONG(K).NE(6.1))
28 CONTINUE
   GO TO 29
   ENTRY READNE
   READ(8.2)(K.[NE(J.K].J=1.8].[=1.N)
29 CONTINUE
   [F([DBUG( 5).NE.0]
  *WRITE(6.1)DMIN
   IF(108UG( 5).NE.0)
  *WRITE(6.2)(1.(NE(J.I).J=1.8).I=1.N)
   RETURN
   END
```

```
SUBROUTINE NEWRAP(T.P.A.B.C.N1,N2.N3)
   IMPLICIT REAL *8(A-H,O-Z)
  REAL #8 NI, N2, N3, J
 1 FORMAT( O FAILED TO CONVERGE IN NEWRAP T= . 1PE12.5.
  #E12.5,5X, 'PO=',E12.5/6X,'A=',E12.5,6X,'8=',E12.5,6X,
  **C=*.E12.5.5X.*N1=*.E12.5.5X.*N2=*.E12.5.5X.*N3=*.
  ₩E12.5)
   TO=T
  PO=P
  DO 22 [=1.50
   SINT=DSIN(T)
  COST=DCOS(T)
   SINP=DSIN(P)
  COSP=DCOS(P)
  F=A+T+B+P-C
  G=N1 *COST *COSP+N2 *SI NT+N3 *COST *SINP
  DGT=-N1 *S1 NT *CQSP+ N2 *CQST - N3 *S I NT *S I NP
  DGP=-N1*COST*SINP+N3*COST*COSP
   J=A +DGP-B+DGT
   TN=T-{F +DGP-G+8}/J
  PN=P+(F+DGT-G+A)/J
   IF(DABS((T-TN)
                 ).GT.1.D-6)
                               GO TO 21
   IF(DABS((P-PN)
                  ).LE.1.0-6)
                               GO TO 23
21 CONTINUE
   IF(I.EQ.50) GO TO 22
   T=0.500*(T+TN)
  P=0.5D0+(P+PN)
22 CONTINUE
   WRITE(6,1)T.TN.P.PN.TO.PO.A.B.C.N1.N2.N3
  CALL ERRWCA
   STOP
23 CONTINUE
   T=TN
  ₽≠PN
  RETURN
  END
```

```
SUBROUTINE NORMAL(X,Y,Z,A,B,C,N1,N2,N3,IT,IB)
   IMPLICIT REAL+8(A-H-0-2)
  REAL #4 ZC . XC . YC
  COMMON /GEOM/2C(50) .XC(50.50) .YC(50.50) .NS.NP
  REAL+8 N1.N2.N3
  COMMON/IDEBUG/IDBUG(80)
  REAL *8 F(3.5).FA(5).FB(5).FC(5)
1 FORMAT('0 NORMAL X='.1PE12.5.5X."Y='.E12.5.5X."Z='.
  *E12.5.5X.2HA=.E12.5.5X.*B=*.E12.5.5X.*C=*.E12.5)
2 FORMAT(8X.'T1',12X,'T2',12X,'A2',12X,'B2',12X,'C2',
  #12x, 'N1 ',12x, 'N2 ',12x, 'N3 '/1 P8E14.5)
   [F(ID8UG(11).NE.0)
  +WRITE(6.1) X.Y.Z.A.B.C
   NSM=NS-1
  DG 21 I=2.NSM
   IF(Z.LE.ZC(1)) GC TO 22
21 CONTINUE
   I=NSM
22 CONTINUE
   CALL BDYFIT(A1.B1.C1.XC(1.I-1).YC(1.I-1).IB.IT1)
   CALL BDYFIT(A2.B2.C2.XC(1.I ).YC(1.I ).IB.IT2)
   CALL BDYFIT(A3,83,C3,XC(1,1+1),YC(1,1+1),IB, ET3)
   IF(IT2.EQ.4) GC TO 23
   IF((IT1.LE.IT2).AND.(IT3.LE.IT2)) GO TO 24
   GO TO 27
23 CONTINUE
   IF((IT1.NE.IT2).OR.(IT3.NE.[T2)) GO TO 27
24 CONTINUE
   FAC 1=1.D0/(ZC(I 1-ZC(I-1))
   FAC 2=1.D0/(ZC(I+1)-ZC(I-1))
   FAC3=1.D0/(ZC(I+1)-ZC(I ))
   FAC4=ZC([-1]+ZC([)
   A2=(A2-A1) #FAC1
   B2=(B2-81) *FAC1
   C2=(C2-C1)*FAC1
   A3={A3-A1}*FAC2
   B3=(83-81) *FAC2
   C3=(C3-C1) +FAC2
   A3=(A3-A2) *FAC3
   83=(83-82) *FAC3
   C3={C3-C2} *F AC3
   A2=A2-A3*FAC4
   82=82-B3*FAC4
   C2=C2-C3*FAC4
   A1=A1-(A2+A3*ZC(I-1))*ZC(I-1)
   B1=B1-(B2+B3+ZC(I-1))+ZC(I-1)
   C1=C1-(C2+C3+ZC(1-1))*ZC(1-1)
   AX=A1+(A2+A3+Z)+Z
   8Y=B1+(B2+B3*Z)*Z
   IF([T2.NE.4] GO TO 25
```

```
N2=-2.D0+(X-A1-(A2+A3+Z)+Z)
   N2=-DABS(N2) *DSIGN(1.DO.X-AX)
   N3=-2.D0+(Y-B1-(B2+B3+Z)+Z)
   N3=-DABS(N3) +DSIGN(1.D0.Y-BY)
   N1=-N2*(A2+2.D0*A3*Z)- N3*(B2+2.D0*B3*Z)+C2+2.D0*C3*Z.
   GD TO 26
25 CONTINUE
   N2=-DABS(AX) +DSIGN(1.DO.X-AX)
   M3=-DABS(BY) *DSIGN(1.D0.Y-BY)
   N1 = -(A2+2.D0+A3+Z)+X-(B2+2.D0+B3+Z)+Y+(C2+2.D0+C3+Z)
26 CONTINUE
   D=D SQRT(N1 ++2+N2 ++2+N3 ++2)
   N1 = N1 /D
   N2=N2/D
   N3=N3/D
   IF(IDBUG(11).NE.0)
  *WRITE(6.2) T1.T2.A2.82.C2.N1.N2.N3
   RETURN
27 CONTINUE
   IF(IT1.EQ.4) GO TO 29
   F(1.1)=0.D0
   F(1.2)=A1
   F(1.3)=0.00
   F(1.4)=81
   F(1.5)=C1
   GO TO 30
29 CONTINUE
   F(1.1)=1.D0
   F(1,2)=-2.00*A1
   F(1.3)=1.D0
   F(1.4)=-2.00*B1
   F(1.5)=C1-A1++2-81++2
30 CONTINUE
                 GO TO 31
   IF( (T2.EQ.4)
   F(2.1)=0.00
   F(2.2)=A2
   F(2.3)=0.00
   F(2,4)=B2
   F(2.5)=C2
   GO TO 32
31 CONTINUE
   F(2-1)=1-00
   F(2.2)=-2.00*A2
   f(2.3)=1.00
   F(2,4)=-2.DQ*B2
   F(2,5)=C2-A2++2-B2++2
32 CONTINUE
                 GO TO 33
   IF(IT3.EQ.4)
   F(3,1)=0.00
   F(3,2)=A3
```

```
F(3.3)=0.00
   F(3,4)=B3
   F(3.5)=C3
   GD TO 34
33 CONTINUE
   F(3.1)=1.D0
   F(3.2) =- 2.D0 + A3
   F(3.3)=1.00
   F(3.4)=-2.00*83
   F(3.5)=C3-A3++2-B3++2
34 CONTINUE
   DZ21=Z2-Z1
   DZ31=Z3-Z1
   DZ 32=Z3-Z2
   Z12=Z1+Z2
   DO 35 K=1.5
   FB(K)=(F(2.K)-F(1.K))/DZ21
   FC(K) = ((F(3.K)-F(1.K))/DZ31-FB(K))/DZ32
   FB(K)=FB(K)-FC(K) *212
   FA(K)=F{1,K}-(FB(K)+FC(K)+Z1)+Z1
35 CONTINUE
   N2=2.DD#(FA(1)+(FB(1)+FC(1)#Z)#Z)#X+FA(2)+(FB(2)+FC(2)#Z)#Z
   N3=2.D0*(FA(3)+(F8(3)+FC(3)*Z)*Z)*Y+FA(4)+(F8(4)+FC(4)*Z)*Z
   N1=-(FB(1)+2.D0*FC(1)*Z)*X**2-(FB(2)+2.D0*FC(2)*Z)*X
      -(F8(3)+2.D04FC(3)4Z)4Y4+2-(F8(4)+2.D04FC(4)+Z)4Y
      +(FB(5)+2.D0*FC(5)*Z)
   AX=FA(1)+(FB(1)+FC(1)*Z)*Z
   IF(AX.EQ.0.D0) AX=-2.D0.
   AX=-2.D0*(FA(2)+(FB(2)+FC(2)*Z)*Z)/AX
   BY=FA(3)+(FB(3)+FC(3)+Z)+Z
   IF(BY.EQ.O.DO) 8Y=-2.DO
   BY=-2.D0+(FA(4)+(FB(4)+FC(4)+Z)+Z)/BY
   N2=-DABS(N2)+DSIGN(1.D0.X-AX)
   N3=-DABS(N3) +DSIGN(1.00 ,Y-BY)
   GO TO 26
   END
```

```
SUBROUTINE OUTPUT(IT)
  COMMON /TITLE/HEAD(20)
  COMMON/VALUE/ZE.X(1000),Y(1000),P(1000),RHO(1000) ,
  #Q(1000).THETA(1000).PSI(1000).N
  COMMON /STAG/PTG(1000).TTG.ATGT.ZG.ZMAX.NB(200).
  *NBO(200), JMAX, JPT, (B, IPLOT, IT11, IT12
  COMMON /GAS/G.RO.GM1.GM1H.GM1G.GGM1.GP1.GPGM
  INTEGER#2 NB.NBC
 1 FORMAT( 11 . 20X . 20A4 / / 30X , 'ZE = 1 . 1 PE12 . 5 . 15X , 'STEP NO . '
 **!5//2X,*NO.*.8X,*X*.14X.*Y*.14X,*P*,13X.**RHO*.13X.*Q*
  *+12X. "THETA ".11X. "PSI ".13X. "M".8X. "BODY "//)
 2 FORMAT(1X,[4,1P8E15,5,1X,A4)
 3 FORMAT(!1:,20X,20A4//10X,'BODY POINTS AT ZE = :,1PE12.5
 **15X**STEP NO.**I5//2X**NO.**8X**X**14X**Y**14X**P**
 *13X.*RHQ*.13X.*Q*.12X.*THETA*.11X.*PSI*.13X.*M*//)
 4 FORMAT(1x.14.198E15.5)
  DATA NES/ YES!/,NO/
  DIMENSION XP(1002) .YP(1002)
  DATA X0/0.0/.DX/25.0/.YG/10.0/.DY/5.0/
   IF(IPLOT.EG.0) GO TO 21
  F=0.0
 . DO 20 [=1.N
  XP(I)=F
   YP([]=P([]
  F=F+1.0
20 CONTINUE
   XP(N+1)=XC
   XP(N+2)=DX
   YP(N+1)=YC
   YP(N+2)=DY
  CALL AXIS(0.0.0.0.*POINT*.-5.14.0.0.0.X0.DX.10.0)
  CALL AXIS(0.0.0.0.P'.1.10.0.90.0.Y0.DY.10.0)
  CALL LINE (XP.YP.N.1.0.1)
  CALL SYMBOL(8.0.8.0.0.15.'STEP '.0.0.5)
  CALL NUMBER (999.0.999.0.0.15.FLOAT (IT).0.0.-1)
   CALL CALCMP(0.0.0.0.0.0.2)
21 CONTINUE
   IF([T11.EQ.0) GO'TO 22
   *THETA( J) .PSI( J) .PTC( J) .J=1 .N}
22 CONTINUE
   IF(IT12.EQ.0) GO TO 24
   WRITE(12)ZE.N.18.NB.NBC
   DO 23 J=1.18
   K=NBO(J)
   WRITE(12)X(K)*Y(K)*P(K)*RHO(K)*Q(K)*THETA(K)*PSI(K)
23 CONTINUE
24 CONTINUE
   IF(JPT.EQ.1) GO TO 25
   [F(([T.EQ.JMAX).OR.(ZE.EQ.ZMAX)) GO TO 25
```

```
IF(MOD(IT.JPT).NE.O) RETURN
25 CONTINUE
  L≠1
  DO 28 J=1.N.50
   N2=J+49
   IF(N2.GT.N) N2=N
   WRITE(6.1)HEAD.ZE.IT
   00 27 K=J.N2
   SM=Q(K)/SQRT(G*P(K)/RHU(K))
   IF (NB(L).NE.K) GO TC 26
   IN=NES
   L=L+1
26 CONTINUE
   WRITE(6,2)K,X(K),Y(K),P(K),RHO(K),Q(K),THETA(K),
  *PSI(K) .SM.IN
27 CONTINUE
28 CONTINUE
   WRITE(6,3)HEAD.ZE.IT
   DO 29 J=1.1B
  K=NBO(J)
   SM=Q(K)/SQRT(G+P(K)/RHQ(K))
   WRITE(6.4)K.X(K).Y(K).P(K).RHO(K).Q(K).THETA(K).
  *PSI(K) .5N
29 CONTINUE
   RETURN
   END
```

```
SUBROUTINE SIMQ(A.R.M.N)
      IMPLICIT REAL +8(A-H-O-Z)
      DIMENSION A(1),R(1)
      DATA EPS/1.D-5/
                  SINGULAR MATRIX IN SIMQ*)
  111 FORMAT('0
      IF(M)23.23.1
C
      SEARCH FOR GREATEST ELEMENT IN MATRIX A
    1 [ER=0
      PIY=0.00
      M*M=MM
      NM=N*M
      DO 3 L=1.MM
      TH=DABS(A(L))
      [F(TB-PIV)3.3.2
    2 PIV=TB
      I=L
    3 CONTINUE
      TOL≃EPS*PI V
C
      A(I) IS PIVOT ELEMENT. PIV CONTAINS /A(I)/.
c
      START ELIMINATION LOOP
      LST=1
      DO 17 K=1.M
C
      TEST ON SINGULARITY
      IF(PIV)23.23.4
    4 IF(IER)7.5.7
    5 IF(PIV-TOL)6.6.7
    6 IER=K-1
    7 PIVI=1.DO/A(I)
      J=(I-1)/H
      X-#*L-1=1
      J=J+1-K
      I+K IS ROW-INDEX. J+K COLUMN-INDEX OF PIVOT ELEMENT
C
C
      PIVOT ROW REDUCTION AND ROW INTERCHANGE IN R.
      DO 8 L=K.NM.M
      LL=L+I
      TB=PIVI*R(LL)
      R(LL)=R(L)
    8 R(L)=18
      IS ELIMINATION TERMINATED
C
      IF(K-M)9,18,18
C
      COLUMN INTERCHANGE IN MATRIX A
    9 LEND=LST+M-K
      IF(J)12.12.10
   10 II=J*M
      DO 11 L=LST.LEND
      TB=A(L)
      LL=L+II
      A(L)=A(LL)
   11 A(LL)=TB
C
      ROW INTERCHANGE AND PIVOT ROW REDUCTION IN MATRIX A
```

```
12 DO 13 L=LST.MM.M
      LL=L+I
      TB=PIVI *A(LL)
      A(LL)=A(L)
   13 A(L)=TB
      SAVE COLUMN INTERCHANGE INFORMATION
C
      A(LST)=J
      ELEMENT REDUCTION AND NEXT PIVOT SEARCH
C
      PI V=0.00
      LST=LST+1
      DO 16 II=LST.LEND
      (II)A-=IVIA
      IST=I(+M
      J=J+1
      DO 15 L=IST.MM.N
      ĹL=L-J
      A(L)=A(L)+PIVI+A(LL)
      TB=DABS(A(L))
      IF ( TB-PI V) 15,15,14
   14 PIV=TB
      15 CONTINUE
      00 16 L=K.NM.M
      LL=L+J
   16 R(LL)=R(LL)+PIVI+R(L)
   17 LST=LST+M
      END OF ELIMINATION LOOP
C
      BACK SUBSTITUTION AND BACK INTERCHANGE
   18 IF(M-1)23,22,19
   19 [ST=MM+M
      LST=M+1
      DD 21 I=2.M
      II=LST-I
      IST=IST-LST
      L=1ST-M
      L=A(L)+0.500
      DO 21 J=II.NM.M
      TB=R(J)
      LL≠J
      DO 20 K=IST.MM.M
      LL=LL+1
   20 TB=TB-A(K) +R(LL)
      K=J+L
      R(J)=R(K)
   21 R(K)=TB
   22 RETURN
C
      ERROR RETURN
   23 IER=-1
      WRITE(6.111)
      STOP
      END
```

```
SUBROUTINE SOLVBP(x.y.A.B.C.A1.B1.C1.IT.x1.Y1)
   IMPLICIT REAL+8(A-H,O-Z)
 1 FORMAT('O NEGATIVE RADICAL IN SOLVEP')
   GD TO(21.22.23.24).IT
21 CONTINUE
   X=C I
   Y=(C-A+X)/B
  RETURN
22 CONTINUE
   Y=C 1
   X=(C-B*Y)/A
   RETURN
23 CONTINUE
   Y=(A+C1-C+A1)/(A+B1-B+A1)
   X=(C-8+Y)/A
   RETURN
24 CONTINUE
   IF(DABS(B).GT.DABS(A)) GO TO 26
  D1=1.D0+(B/A) ++2
   D2=C/A-A1
   D3=(D2++2+B1++2+C1)/D1
  D2=(B+D2/A+B1)/D1
  RAD=D2**2-D3
   IF(RAD.GE.O.DO) GO TO 25
   WRITE(6.1)
   WRITE(6.2)X,Y.A,B.C.A1.B1.C1.IT.X1,Y1.D1.D2.D3
 2 FORMAT( '0 X= +.1PE12.5.5X. "Y= +.E12.5/3X. A= +.E12.5.5X.
- + B= -.E12.5.5x, C= -.E12.5/2x, A1=-.E12.5, 4x, B=-.E12.5.
  *4 X. *C1=*.E12.5/2X.*IT=*.I2.14X.*X1=*.E12.5.4X.*Y1=*.
  *E12.5/2X.*D1=*.E12.5.4X.*D2=*.E12.5.4X.*D3=*.E12.5)
   CALL ERRWCA
   STOP
25 CONTINUE
   RAD=DSQRT(RAD)
   Y=D2+RAD
   IF(DABS(Y1-Y).GE.DABS(Y1-D2+RAD)) Y=D2-RAD
   X={C-B*Y}/A
   RE TURN
26 CONTINUE
   D1=1.D0+(A/B) **2
   D2=C/8-81
   D3=(D2++2+A1++2-C1)/D1
   D2=(A+D2/B+A1)/D1
   RAD=D2 **2-D3
   IF(RAD.GE.0.DO) GO TO 27
   WRITE(6.1)
   WRITE(6.2) X.Y.A.B.C.A1.B1.C1.IT.X1.Y1.D1.D2.D3
   CALL ERRWCA
   STOP
27 CONTINUE
```

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RAD=DSQRT(RAD)

X=D2+RAD

IF(DABS(X1-X).GT.DABS(X1-D2+RAD)) X=D2-RAD

Y=(C-A+X)/B

RETURN

END

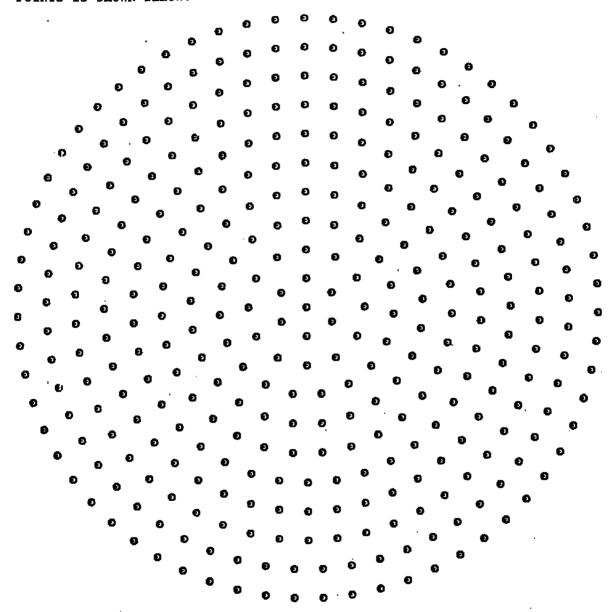
```
SUBROUTINE SORT (DN.NE.N)
   DIMENSION DN(N)
   INTEGER+2 NE(N)
   N1 =1
   N2≖N
20 CONTINUE
   DMIN=DN(N1)
   DMAX=DN(N2)
   IF(DMIN.LE.DMAX) GO TO 21
   D=DN(NI)
   DN(N1)=DN(N2)
   DN(N2)=D
   N=NE(N1)
   NE(N1)=NE(N2)
   NE(N2)=M
   GO TO 20
21 CONTINUE
   N1=N1+1
   N2=N2-1
   IF(N1.GT.N2) GO TO 24
   DO 23 I=N1.N2
   IF(DN(1).GE.DMIN) GO TO 22
   DN(N1-1)=DN(I)
   DN(I)=DMIN
   DMIN=DN(NI-1)
   M=NE(I)
   NE(I)=NE(N1-1)
   NE(NI-1)=M
   GO TO 23
22 CONTINUE
   IF(DN(I).LE.DMAX) GO TO 23
   DN(N2+1)=DN(1)
   DN(I)=DMAX
   DMA X=DN( N2+1)
   M=NE([)
   NE( I ) = NE( N2+1)
   NE (N2+1)=M
23 CONTINUE
   GO TO 20
24 CONTINUE
   RETURN
   END
```

```
SUBROUTINE THREED
  COMMON/VALUE/ZE.X(1000).Y(1000).P(1000).RHO(1000) .
 *Q(1000).THETA(1000).PSI(1000).N
  COMMON /GAS/G.RO.GM1.GM1H.GM1G.GGM1.GP1.GPGM
  COMMON/NVALU/DZ.XN(1000).YN(1000).PN(1000).RN(1000).
 *QN(1000).TN(1000).PSN(1000)
  COMMON /BCUT/X8(50) .YB(50)
  COMMON /OCUT/X80(50) 4Y80(50)
  COMMON /STAG/PTO(1000),TTO.ATOT.ZO.ZMAX.NB(200).
  *NBO(200).JMAX.JPT .IB
   INTEGER#2 NB ,NBC
  REAL #8 ZD.DG.DRC.DGM1.DGM1H.DGM1G.DGGM1.DGP1.DGPGM
  COMMON /DGAS/ZD.DG.DRO.DGMI.DGMI.DGMIG.DGMI.DGPI.
  *DGPGM
  REAL*8 PTOD.TTOD.ATOD
  COMMON /DSTAG/PTOD(1000),TTOD,ATOD
  DO 19 [=1.N
   PTOD([)=PTC([)
19 CONTINUE
   TTOD=TTN
   A TOD = A TOT
  າG≔G
  DRO=RO
  DGM1=DG-1.DO
   DGM1H=0.5D0+DGM1
   DGM1G=DGM1/DG
   DGGM1=1.DO/DGM1G
   DGP1=DG+1.DO
   DGPGM=DGP1/DGM1
   CALL CUT(ZO)
   ZE=ZO
   DO 20 I=1.50
   XBO(1)=XB(1)
   YBO(1)=YB(1)
20 CONTINUE
   D0 26 J=1.JMAX
   CALL OUTPUT(J-1)
   CALL DIST(DS)
   DZ= 0.5*DS
   IF ((ZE+DZ).LE.ZMAX) GO TO 21
   IF(ZE.GE.ZMAX) RETURN
   DZ =Z MA X-ZE
21 CONTINUE
   ZO = DZ
   CALL CUT(ZE+DZ)
   DO 23 I=1.N
   CALL FIT(I)
   (F(NB(K).EQ. I) GO TO 22
   CALL FIELD(I)
```

GD TO 23 22 CONTINUE CALL BODY(1) K=K+1 23 CONTENUE ZE=ZE+DZ DO 24 I=1.N X(T)=XN(T)Y(I)=YN(I)P(I)=PN(I)RHO(I)=RN(I) Q(I)=QN(I)THETA(I)=TN(I) PSI(I)=PSN(I) 24 CONTINUE DO 25 1=1.50 (1)8x=(1)08x Y80(I)=Y8(I) 25 CONTINUE 26 CONTINUE CALL GUTPUT(JMAX) RE TURN END

APPENDIX B EXAMPLE PROBELM

THE SAMPLE PROBLEM IS FOR M = 4.1 AXISYMMETRIC NOZZLE WITH GAMMA = 1.2. THE NOZZLE AXIS IS ALIGNED WITH THE Z AXIS. THERE ARE 48 STATIONS FOR THE BODY GEOMETRY. THE STARTING PLANE INPUT HAS ONE RAY WITH 11 POINTS. THE COMPLETE STARTING PLANE IS GENERATED FROM THESE 11 POINTS TO A TOTAL OF 346 NEARLY EQUALLY SPACED POINTS. THE ARRANGEMENT OF THESE POINTS IS SHOWN BELOW.



IMPUT CARDS


```
WACH & MOZZLE (G=1.24)
 45
 36
       3 9.205
1.01532 0.0
 36
       3 0.25
1.02200 0.0
 36
       3 0.30
1.03344
 36 . 3 0.35
1.04594
        9-0
 36
      3 0.40
1-06051 0-0
 36
      3 0.45
1.07710
        0.0
 36
1-09561
        0.0
 30
      3 0.55
1-11586 0-0
       3 0.60
 36
1-13762 0.0
 36
       3 D.65
1.16058 0.0
 36
       3 0.70
1.18442 0.0
 36
       3 0.80
1.23355
        0.0
 36
       3 0.90
1.28315
 36
       3 1-00
1.33273 0.0
 36
       3 1-10
1.38226 . 0.0
 36
       3 1.20
1.43171 0.0
 36
       3 1.30
1.48105 0.0
 36
      3 1.40
1.53026
        0.0
 36
      3 1.50
1.57936
        0.0
 36
      3 1.60
1-62631
        0.0
 36
      3 1.70
1.67711 0.0
 36
      3 1.80
1.72574 0.0
 36
       3 1.93260
1.78990 0.0
 36
      3 2.09378
```

1710.0

4-97416 0-0

100 a D

100.0

1.24

INPUT CARDS

205	24.0	•	1 11	36 10D 10a	ı		
0.0	9.0	55.035	1.0105	ð. á	0.0	0.0	0
0.10153	0.0	54.887	1 - 01 291	0.22466	0.0	0.0	0
9 - 20 306	0.0	54.439	1.02022	9.47544	7-0	0.0	ō.
0.30460	0.0	53,676	1.03271	0. 77981	9-0	0.0	0
9.40613	0.6	52.571	1 - 05091	1.16897	0.0	0.0	0
9-50766	0.0	51.079	1.07571	1.68158	0.0	3 .O	
0-60919	0.0	494127	1.19859	2.36939	0.0	0.0	
6.71072	9.0	46.613	1.15183	3.30375	0.0	0-0	0
9-81226	0.0	43,385	1.20905	4.58134	0.0	0.0	0
0:91379	0.0	39,245	1-28600	6.32552	0.0	0.0	0
1-01532	0.0	33.953	1.39203	5.67814	0.0	0.0	1

MACH & NOZZLE (G=1.24)

STARTING PLANE INPUT

GAMMA =1.240	PT0 = 1.00000	02	TTO - 1.00000E	02 R = 1.71600E 03		
ZD= 2.05000E-01	ZMAX= 2.400000	01		V= 1 NPTS= 11 1= 0 IT12= 0	MRAYS= 36 [NEIGH= 0	JMAX= 100 JPT= 100
×	7	P	Q	THETA	PST	PTO

NO. x p exo. THETA ۵ 289 BODY • 0.0 0.0 5.50350E 01 3-60015E-04 4-39952E 02 0.0 1.01050E 00 1.015306-01 0.0 5.48870E 01 3.59234E-04 4.40887F 02 3-92105E-03 0.0 1-012916 00 5.07651F~02 8.79274E-02 5-48870E 01 3.59234E-04 4.40887E 02 1-96053E-03 3-395736-03 1-01291E 00 -5.07648E-02 8.79276E-02 5.48870F 61 3.59234E+04 4.40887E 02 -1.96052F-03 3.39874E-03 1.01291E 00 -1.01530E-01 1.605 79F - 07 5-48870F 01 3-59234F-04 4-201555-09 4.40887E 02 -3.921 ase-as 1-01291E 00 -5.97651E-02 -8.79274F-02 5.48879E 01 3-59234E-04 4.40BB7E 02 -1.96053E-03 -3.396736-03 1-81291F 40 5-07648E-02 -B. 79276E-02 5.4887QE QL 3.59234E-04 4.40887F 02 1-98052E-03 -3.39574E-03 1.01291E 00 2.03060F-01 0.0 5.44390E GL 3.56867E-04 4.43717F 02 B-29798E-03 0.0 1.02022E 06 1.758556-01 1.015306-01 5.44390F 01 3.56667E-04 4.43717E D2 7-18623E-03 4-14905E-03 1.02022E 00 10 1.01530E-01 1.75855E-01 5-44390F 01 3-56867E-04 4-43717E 02 4. L4896F-03 7-186295-03 1.02022E 00 11 2.57403E-07 2.03060E-01 5.44390E 01 3.56867E-04 4.43717E 02 1.05185E-08 5.29798E-03 1.02022E 00 12 -1-01530E-01 1.75855E-01 5.44390E 01 -3 - S6867F-0A 4.43717E 02 -4.14894E-D3 7.18630E-03 1.02022E 86 13 -1.75855E-Q1 1-01530E-01 5.44390E 01 3-56867E-04 4,43717E 02 -7-186236-03 4.149077-03 1.02022E 00 14 -2.03060E-01 3421159E-07 5.44390E Ot 3.56867E-04 4.43717E 02 -8.29798E-03 1.31244E-08 1.02022E 00 15 -1.7585SE-01 -1.01530E-01 5.44390E OL 3.56867E-04 4.43717E 02 -7-18624E-03 -4-14905E-03 1-02022E 00 -1.01530E-01 -1.75A5SE-0L 5.44390E 01 3.56867E-04 4.43717E 02 -4-14896E-D3 -7-18629E-63 1.020226 00 17 -3.84916E-07 -2.03060E-01 5.44390E 01 3.56867E-04 4.43717E 02 -1.57293E-08 -6.29798F-03 1,02022E 00 18 1.01530E-01 -1.75855E-01 5.44390E 01 3.56867F+04 4.43717E 02 4.14893E-03 -7.18630E-03 1.02022€ 00 19 1.75655E-01 -1.D:530E-01 5.4439DE Q1 3-56867E-04 4-43717E 02 7.16623E-03 -4,14907E-03 1.02022E 00 20 3.046D0E-01 0.0 5.36760E OL 3.52828E-04 4.48536E 02 1.36102E-02 0.0 1.03271E 00 21 2.68096E-01 9.89033E-02 5.36760E OL 3.52828E-04 4.48536E 02 1.28728E-02 4.41947E-03 1.03271E 00 22 2.40372E-01 5.36760E 01 1.87089E-01 3.52828E-04 4.48536E 02 1.07403E-02 6.359896-03 1.0327LE 00 23 1.66601E-01 2.5500 1E-01 5.36760E DI 3.52828E-64 4.48536E 02 7.44394E-03 1-139426-02 1.03271E 00 24 7-477548-02 2.95279E-01 5.3676DE DI 3.52828F-04 4.48536E 02 3.34104E-03 1.31938E-02 1-03271E 00 25 -2-51531E-02 3.93560E-01 5.36760E 01 3.52828E-04 4-48536E 02 -1.12387E-03 t.35636E+02 1.03271E 00 26 -1-22356E-01 2.78945E-D1 5.36760E 01 3.52828E-04 4.48536E 02 -5.46699E-03 L.24640E-DZ 1.03271E 00 -2-06299E-01 2-241 02E-01 5.36760E D1 3.52826E-04 4.48536E D2 -9.217786-03 1.00137E-02 1-03271E 00 28 -2.67887E-01 1.44974E-01 5.36760E 01 3.52828E-04 4.48536E 02 -1-19697E-02 6.478195-03 1.03271E 00 29 -3.00445E-01 5.01366E-02 5.36760E 01 3.52828E-04 4.48536E 02 -1.34246E-02 2.240358-03 1.03271E 00 30 -3.00446E-01 -5.01345E-02 5.36760E 01 3.52828E-04 4.48536E 02 -1.342466-02 -2.24026E-03 1.03271E 70 31 -2.67888E-01 -1.44972E-01 5.2676QE Q1 3.52828E-04 4.48536E 02 -1-19698E-02 -6.47861E-03 1.03271E 00 32 -2.06301E-01 -2.24101E-01 5.36760E 01 3.52828E-04 4.48536E 02 -9.21784E-03 -1.00136E-02 1.03271E DO 33 -1.223586-01 -2.78944E-01 5.36760E D1 J.52826E-04 4.48536E 02 -5.46708E-03 -1-246405-02 1.03271E 00 34 -2.51555E-32 -3.03559E-01 5.36760E 01 3.52828E-04 4.48536E 02 -1.12397E-03 -1.35637E-02 1.03271E GO 35 7.47725E-02 - 2.95280E- D1 5.36760E 01 3.52828E-04 4-48536E 02 3.340916-03 -1.31938E-02 1.032714 00 36 1.66599E-01 -2.55002E-01 5436760E 01 3,52828E-04 4.485362 02 7.44386E-Q3 -1.13943E-02 1.032716 00 37 2.43371E-01 -1.87091E-01 5.36760E 01 3.52828E-04 4.45536E 02 1-07402E-02 -8.35998E-03 1.03271E 00 38 2.88095E-D1 -9.89060E-02 5.36760E 01 3-52625E-04 4.48536E DZ 1.26727E-02 -4-41960E-03 1.03271E 00 39 4.061306-01 0.0 5.2571 OE 01 3.46959E-04 4.55523E -02 2-04024E-02 0.0 1.05091E 00 40 3.93371E-01 1.010D0E-01 5.25710E 01 3.46959E-04 4.55523E 02 1-9761 3E-02 5.07451E-03 1.05091E 00 41 3.55894E-01 1.956546-01 5.25710E 41 3.469596-04 4.55523E 02 L.78784E-02 9-82995E-03 1.05091E 00 42 2,96056E-01 2.78015E-01 5.2571 OE 01 3.46959E-04 4.55523F 02 1.467ZZE-02 1.396748-02 1.05091E 02 43 2-17615E-01 3.42907E-01 5.2571QE 01 3.46959E-04 4.555232 02 1.093156-02 1.72270E-02 1.05091E 00 44 1 - 25502E-01 J.86252E-01 5.2571QE 01 3.46959E-04 4.55523E 02 6.30430E-03 1-94040E-02 1.05091E 00 45 2.55016E-Q2 4.05329E-01 5-2571 OE 01 3.46959E-Q4 4.55523E 02 1.28101E-03 2.03621E-02 1.050918 00 46 -7.61006E-02 3.98936E-01 5.25710E 01 3.46959E-04 4.55523E 02 -3.82274E-03 2.00411E-02 1.05091E 00 47 -1.72921E-01 3.67478E-01 5.2571 QE 01 3.46959E-04 4-55523E 02 -8.68638E-03 1.64611E-02 1.05091E 00 48 -2.58877E-01 7.12929E-01 5.2571 0E 01 3.46959E-04 4.55523E 02 -1.30044F-02 1.57212E-02 1.050918 00 49 -3-26566E-01 2.387186-01 5.25710E 01 3.469592-04 4.55523E 02 -1.65054E-02 1-19933E-02 1.05091E 00 -3477610E-01 1.49507E-01 5.2571 QE 01

3.46959E-04

4.95523E 02

-1.89694E-02

7.51154E-03

1.05091E 00

MACH 4 NOZZLE (G=1.24)

ZE = 2.05000E-01

STEP NO. D

ND.	x	Y	р	RHO	. 0	THETA	PŠĮ	M	8004
51	-4:02927E-01	5.05022E-02	5.257100 01	3.46959E-04	. 4.55523E 12	-2.02414E-G2	2.55747E-03	1.050915 00	
52	-4.02928E-01	-5.09009E-02	5.25710E 01	3.46959E-04	4.5552JE 02	-2.024156-02	-2.55741E-03	1.05091E 00	
53	-3.776102-01	-1.49506E-01	5.25710E 01	3.46959E-04	4.55523E 02	-1.89695E-02	-7.51146E-03	1.050915 00	
54	-3.28567E-01	-2.18716E-01	5.2571 0 E 01	3.46959E-04	4.55523E 02	-1.65055E-02	-1.19933E-02	1.050915 00	
55	-2.58876E-01	-3.12928E-01	5.25710E 01	3.46959E-04	4.55523E DZ	-1,30044E-02	-1.57211E-02	1-05091E 00	
56	-1.72922E-01	-3.67477E-01	5.25710E 01	3.469592-04	4.55523E 02	-8.68644E-03	-1.84410E-02	1.05091 = 00	
57	-7.61023E-02	-7.98936E-01	5.2571 0 E 01	3.46959E-04	4.55523E 02	-3.62282E-03	-2.90411E-02	1-05091E 00	
56	2.54992F-02	-4.05329E-01	5.25710E QL	3.46959E-04	4.555238 02	1.28089E-03	-2.03621E-02	1.05091E 00	
59	1.254986-01	~3.86253E-01	5.2571 0 F D1	3.46959E-04	4.55523E Q2	6.304 L4E-03	-1.94041E-02	1.05091E 00	
60	2 • 1 761 4C - Ot	- 3 • 4 2908E-01	5.257] QE 01	3.46959E-04	4.55523E 02	1.0931 5E -02	-1.7227QE-02	1.05091E 00	
61	2.96054E-01	-2.78017E-01	5.25710E 01	3.46959E-04	4.55523E 02	1.48721E-02	-1.39675E-02	1.05091E 00	
62	3.SS894E-01	-1,95656E-01	5-2571 0 E 01	3,46959E-04	4.55523E 92	1.78784E-02	-9.83001E-03	1.05091E 00	
6.3	7493370E-01	-1.01602E-01	5.2571 <i>0</i> E Q1	3,46959E-Q4	4-55523E 92	1-97613E-02	~5.07462E-03	1.050918 00	
64	5.07660E-01	0.0	5.10790E 01	3.38996E-04	4.64975E 02	2.93491E-02	0.0	1.07571E 00	
65	4.97268E-01	1.02191E-01	5.10790E 01	3.38996E-04	4.64975E 02	2.87481E-02	5.90955F-Q3	1.075 7 1E 00	
66	4.66518E-01	2.0019BE-01	5.10790E D1	3.38996E-04	4.64975E 02	2.697002-02	1.1576#E-02	1.07571E 70	
67	4.156696-01	2.900100-01	5.197 902 01	3.38996E-Q4	4.64975E 02	2.4Q875E-02	1.676945-02	1.07571E 00	
68	3.49761E-01	3.67948E-01	5.1079 0 F 01	3.38996E-04	4.64973E D2	2.02190E-02	2,12749E-02	1.0757LE 00	• .
69	2.68534E-01	4.36822E-01	5.10790E 01 .	3.38996E-04	4.64975E 02	1.55230E-02	2.49389E-02	1-075716 00	
70	1.76313E-01	4.76D59E-01	5.1079 0 E 91	3.38996E-04	4.64975E 02	1-01918E-02	2.75231F-02	1.07571E 00	
71	7.68746E-02	5.01806E-01	5.1079 0 0 01	3.36996E-04	4.64975E 02	4.44368E-03	2.90108E-02	1.07571E 00	
72	-2.57118E-02	5.07008E-01	5.1079 0F 01	3.38996E-Q+	4.64975E Q2	-1.486258-03	2.93114E-02	1.07571E 00	
73	-1.27245F- 01	4.91454E- 0 1	5.10790E 01	3.389956-04	4.64975E 02	-7.35538E-03	2.84127E-02	1.07571E 00	
74	-2.23570E-01	4.5578QE-01	5.1079 0 E 01	3.38996E-04	4.64975E Q2	-1.29236E+02	2.63512E-02	1.0757LE 00	
75	-3,1074[E-0]	4.01446E-01	5.1079CE 01	3.38996E-04	4.64975E Q2	-1.7963lE-Q2	2.32111E-02	1.07571E 00	
76	- 3.85191E-01	3.306765-01	3.10790E 01	3.38996E-04	4.64975E 02	-2.22675E-02	1.91204E-D2	1.07571E 00	
77	-4,43870E-01	2.46369E-01	5-10790E 01	3,389965-04	4.64975E 02	-2.30604E-02	1.42463E-02	1,07571E 00	
78	-4.84378F-01	1.51976E-01	5.10790E Bl	3.3 89 96E-04	4.64975E 0 2	-2.80027E-02	8.78839E-03	1.07571E 00	
79	-5.05055E-01	5.13671E-02	2.10790E OL	3.38996E-04	4.64975E Q2	-2.91985E-02	2.9701 0 E-03	1.07571E 00	
80	-5.05055F-01	~ 5. 13581 E~ 0 2	5.10790E 01	3.38996E-04	4.64975E 02	-2.91985E-02	-2.9699 8 F-03	1.07571E 00	
81	-4.84379E-01	-1.51974E-01	5.10790E 01	3.38996E-04	4.64975E 02	-2.6002 4 E-02	-8.78827E-01	1.07571E 00	
82	-4.438712-01	~ Z. 46367E~ 01	5-1079QE 01	3,38996E-04	4.64975E QZ	-2,56604E-02	-1.42462E-02	1.07571E 00	
83	-7.65192E-01	– I. 30675F– 01	3.10790E 01	3.38996E-04	4.64975E 02	-2,226 <i>7</i> 9E-D2	~1,91203E-D2	1.07571E 00	
64	-3.10742E-01	-4.01445E-01	5.10790E 01	3.38996E-04	4.64975E 02	-1.79632E-02	-2.32110E-02	1,07571E 00	
65	-2.235726-01	-4.55779E-01	5-1079 0 E 01	3,38996E-Q4	4.64975E 02	-1.29237E-02	-2.6351 <i>2</i> E-02	1.07571E 00	
86	-1.27247E-01	-4.914546-01	5.1079 0 E 01	3.38996E-04	4.64975E Q2	-7.35547E-03	-2,84127E-02	1.07571E 00	
-57	-2.57144E-D2	-5.07 008E-0 1	5.1079 0E 0 1	3.38996E-04	4.64975E Q2	-1.4864QE-Q3	-2.93114E-02	1.07571E 00	
86	7.68710F-02	-5.01606E-01	5.10790E 71	3. 38996E-94	4.64978E 02	4.44348E+03	-2.90109E-02	1.07571E 00	
89	1.76311E-01	- 4. 76060E- 01	5.1079 0 E 01	3. 38996E-04	4.64978E 02	1.01917E-02	-2,75232E-02	1.07571E 00	
90	2.6853ZE-01	-4.30824E-01	5.10790E 0]	3.38996E-04	4.64975E Q2	1.55229E-02	-2.49090E-02	1.07571E DO	
91	3.4976QE-01	-3.67949F-01	5.10790E Q1	3.3 8996 E-04	4.64975E 02	2.02190E-Q2	-2.1275GE-02	1.07571E 00	
92	4.16667E-01	+5-90015E-01	5.10790E D1	3.38996E-04	4.64975E 02	2.40874E-02	-1.67696E-02	1.07571E 00	
93	4.66517F-D1	- 2. 00200E-01	5-10790E 01	3.38996E-04	4.64975E Q2	2.69699E-02	-1.15769E-02	1.07571E 00	
94	4.97268E-01	-1.02194E-01	5.10790£ 01	3, 38996E-64	4.64975E Q2	2.874812-02	-5 .909702-0 3	1.07571E 00	
95	6.0919QE-01	0.0	4.91270E D1	3.28508E-04	4.77384E Q2	4.13536E-02	0.0	1.108598 00	
96	6.00881E-01	1.00269E-01	4.91270E 01	3.28505E-04	4.77384E 02	4.07893E-02	6.81039E-03	1.106595 00	
97	5.761826-01	1.97603E-01	4.91270E OI	3.28508E-04	4.77384E 02	3.91110E-02	1.343436-02	1.198598 00	
98	5-35767E-01	2.89942E-01	4.91270E 01	3.28508E-04	4.77384E 02	3,63671E-02	1.949965-02	1.10859E 00	
99	4.A0737E-01	3.74172E-01	4.91270E 01	J. 26508E-04	4.77384E 02	3.26303E-02	2,540896-02	1.10659E 00	
100	4 - 1 259 3E - 01	4.4619BE-91	4.91270E 01	3.28508E-Q4	4.77364E 02	2.80037E-02	J.04328E-02	1.106598 90	

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NO.	×	٧	P	RHØ	Q	THETA	PS1	H	BODY
				3. 28508E-04	4.77384E 02			1.10859E 00	
101 102	3.33196E-01	5.09993E-01	4.91270E 01 4.91270E 01	3.28508E-04	4.77384E 02	2.26136E-02 1.66076E-02	3.46256E-02 3.78740E-02	1.108596 00	
102	2.44709E-01 1.49548E-01	5.5788DE-01 5.90549E-01	4.91270E 01	3.28508E-04	4.77384E .02	1.014905-02	4.06896E-02	1.108595 00	
104	5.03070E-02	6,071096-01		J. 26508E-Q4	4,77384E 02	3.414026-03	4.12126E-02	1.10859E 00	
105	-5.03061E-02	6.07109E-01	4.912702 01	3.28508E-04	4.77384E 02	-3.413962-03	4.12126E-02	1.10859E 00	
106	-1.49546E-01	5.90549E-01	4.912702 01	3.28508E-04	4.77384E 02	-1.01489E-02	4.00896E-02	1.10859E 00	
107	-2.44708E=01	5.578B0E-01	4.91270E 01	3,28508E-04	4.77384E 02	-1.66075E-02	3.78741E-02	1-10859£ 00	
108	-3.33195E-01	5.09994E-01	4.91270E 01	3,285062-04	4.773842 02	-2.26137E-02	3.462586-02	1.108596 00	
189	-4.12593E-01	4.481 965-01	4.912705 01	3.2850BE-04	4.77384E 92	-2.60037E-02	3.043292-02	1.10859E DO	
110	-4.80736E-01	3.74173E-01	4.91270E 01	3,28508E-04	4.77384E 02	-3.26303E-02	2.54090E-02	1.10859E 00	
111	-5.35766E-01	2.89943E~01	4.91270E 01	3.285D8E-04	4.77384E 02	-3.6367 02-02	1.9 6909E- 02	1.10859E 00	
112	-5.76182E-01	1.97805E-01	4.91270E 01	3,28508E-04	4.77384E 02	-3.91118E-02	1.34344E-02	1.10859E DO	
113	-6.99881E-01	1-392 70E —91	4.91270E 01	3.28508E - 24	4.77384E 02	-4.07893E-92	6.61042E-03	1.10859E 00	
114	-6.09190E-91	9.63492E-07	4.91270E 01	.3.2850BE-04	4.77384E 02	-4.13536E-02	6.54421E-08	1.108\$9E 00	
115	-6.00882E-01	-1.00268E-01	4.91270E 01	3.28508E-04	4.77384E Q2	-4.07693E-Q2	-6.8103¢E-03	1.10859E 00	
116	-5.761832-01	-1.97802E-01	4.91270E 01	3.28508 E-0 4	4.77384E 02	-3-91118E-02	-1.34343E-02	1.108596 00	
117	-5.35767E-01	-2,89941E-01	4,91270E 01	3-28508E-04	4.77364E 02	-J-6J671E-02	-1-96908E-02	1.108598 00	
118	-4. R0737E-01	-3.741 71E-01	4.91270E 01	3.28508E-04	4.773842 02	~3.26304E~02	-2.54089E-Q2	1.108598 30	
119	-4.12594E=01	-4.48195E-01	4.91270E 01	3,28508E -0 4	4,77384E 02	-2.80038E-02	-3.04328E-02	1.10859E 00	•
120	-3.33197E-01	-5.09992E-01	4.91270E DI	3.285962 -04	4.77384E QZ	-2.26139E-02	-3.46267E-02	1.10859E 00)
121	-2.44710E=01	-5,57879E-01	4.91270E 01	3. 26508E - 04	4.77384E D2	-1.66077E-02	-3.78740E-02	1.10859E 00	
1 22	-1-49549E-01	-5.90549E-01	4.91270É 31	3, 28508E-04	4.77384E Q2	~1.D1491E-02	-4.00896E-02	1.10859E 00	1
123	-5.03103E-02	-6.07109E-01	4.91270E Q1	3.28506E~04	4.77384E 02	-3.41424E~03	-4.12125E+02	1.10859E 00	•
124	5.030516-02	~ 6. 971 09E= 01	4.91270E 01	3.28508E~ 6 4	4.77384E 02	3.41389E-03	-4.12126E-02	1.10559E 00	•
125	1 - 49545E-01	-5.90549E-01	4.91270E D1	3.28508 E-0 4	4.77384E 02	1.01489E-02	-4.006965-02	1.10859€ 00)
126	2.44707E-01	-5.57881E-01	4.91270E 01	3.20508E-04	4.77384E 02	1.66074E-02	-3.78741E-02	1.10859E 00	•
127	3.33192E-01	-5.09995E-01	4.91270E 01	3.28508E-04	4.77384E 02	2.26136E-02	~3.46259E~02	1.10859E 00	
120	4-12590E-01	-4.48198E-01	4.91270E 31	3.26508E-04	4.77384E 02	2.80035E-02	-3.04330E-02	1.10559E 00)
129	4.807356-01	-3.74173E-01	4,91270F 01	3,28508E-04	4,77384E Q2	3.26302E-02	-2,54090E-Q2	1.10859E Q0)
1 30	5-357665-01	-2.89944E-01	4.91270E 01	3.28508E-04	4.77384E 02	3.63670E-02	-1.96910E-02	1,10859E 00	
131	5.76 L8 1E-01	-1.97807E-0L	4.91270E 31	3.28508E-04	4.773848 02	3.91117E-02	-1434346E-02	1.10859E 00	•
132	6-00881E-01	-1.00273E-01	4-91270E 01	3.28508E-04	4.77364E 02	4-07893E-02	-6.81061E-03	1.10859E 00)
133	7.10720E-01	0.0	4.86130E 01	3.14853E-04	4.93489E 0Z	5.76613E-02	0.0	1.15183E 00)
134	7.03486E-01	1.01146E-91	4.66130E 91	3,14863E-04	4.93489E 02	5.70737E-02	8.21497E-03	1.15163E 00	
135	5.8193 LE-01	Z.00233E-01	4.66130E OI	3.14863E-04	4.93489E 02	5.532326-02	1.62616E-02	1.15183E 00	•
136	6.46494E-01	2.95243E-01	4.66130E 01	3.14883E-04	4.93489E 02	5.24455E-02	2.39753E-02	1,15183E 00)
137	5.97896E-01	3.04244E-01	4.66130E DI	3.14683E-04	4.93489E 02	4.849996-02	3-11985E-02	1.15183E 00)
138	5437126E-01	4.654225-01	4.66130E 01	3.14883E-04	4.93489E 02	4.35671E-02	3.77840E-02	1.151838 00	
139	4.65423E-01	5.371266-01	4.66130E DL	3.14883E-04	4.93489E 02	3.77482E-02	4.35982E-02	1.15183E 00	
140	3.84244E-01	5.97895E-01	4.66130E 01	3-14863E-04	4.93489E 02	3.11618E-02	4.85234E-02	1.15163E 00	
141	2.95244E-01	4.46493E-01	4-66130E 01	3,1486JE-04	4.93489E 02	2.39424E-02	5.24605E-D2	1.151838 00	
142	2.00233E-01	4.619316-01	4.56130E 01	3.146532-04	4.93489E 02	1.62368E-02	5.53304E-02	1.15183E 00	
143	1.011476-01	7.034866-01	4.66130F 01	3.14883E-04	4.9 3489E 32	8.20145E-03	5470756E-02	1.15103E 00	
144	9.00922E-07	7.10720E-01	4.66130E D1	3.14803E-04	4.93489E 02	7.30519E-08	5.76613E-02	1.15183E 00	
145	-1.01145E-01	7.03486E-01	4.86130E 01	J.14883E-04	4.93489E 02	-8.2015QE-03	5.70757E-02	1.15183E 00	
146	-2.00237E-01	6.81931E-01	4.661305 01	3.14883E-04	4.93489E 02	-1.62367E-02	5.53395E-02	1,151832 00	
147	-2.95243E-01	6.46494E-01	4.66130E 01	3.14863E-04	4.93489E 02	-2.39423E-D2	5.24606E-02	1.15183E 00	
148	-3.64243E-01	5.97896E-01	4.66130E 01	3.14883E-04	4.93489E 02	-3.11617E-02	4.85235E-02	1.1516JE 00	
149	-4.65422E-01	5.37127E-01	4.66130E 01	3.14863E-04	4.93489E D2	-3.77461E-02	4.35982E-02	1.15183E 00	
150	-5.37126E-01	4.65423E-01	4.66130E 01	3.14883E-04	4.93489E 02	-4.35671E-02	3.7784 E-02	1.15183E 00	
194	-21211505-41	-403463C-RI	## potage or	7114003E-A4	-07J907E UZ	-4.330/16-02	90116416-05	********	

MACH 4 NOZZLE (G=1.74)

ZE = 2.05000E-01 STEP NO. 0

					•				
NO.	x	Y	P	RHD	Q	THETA	PSI	M	BODY
151	-5.97595E-01	3.84245E-01	4.66130E 01	3.14883E-04	4.93489E D2	-4.84998E-02	3.11986E-02	1.15183E 00	
152	-6.46493E-01	2,95245E-01	4.66130F 91	3.14883E-04	4.93489E 02	-5.24455E-02	2.397546-02	1-15183E 00	
1 53	-6.81930E-01	2.00234E-01	4.66130E 01	3-14883E-04	4.93489E 02	-5.53231E-02	1 - 624 18E-02	1-151835 00	
154	-7.03486E-01	1-01147E-01	4.66120E D1	3.14883E-04	4.93489E 02	-5.70737E-02	. 8.21504E-03	1-15183E 00	
1 55	-7.10720E-01	1.12407E-06	4.66139E 91	3.14883E-Q4	4,9 J489E 02	-5.76613E-02	9-12980E-08	1.15183E 00	
156	-7.07486E-01	-1.01145E-01	4.661300 01	3.[4883E-04	4,93489E 02	-5.70737E-02	-B.21486E-03	1.15183E 00	
157	-6.61931E-01	-2.00232E-01	4.6613QE OL	3.14683E-04	4.93469E Q2	-5.53232E-02	-1-62616E-02	1-15163E 00	
156	-6.46494E-01	-2.9524JE-01	4.66130E D1	3.14883E- 0 4	4.93489E 02	-5.244552-02	- 2. 39753E-02	1.15183E 90	
159	-5.97896E-01	~3.84243E-01	4.6613QE D1	J.1483E- 0 4	4.93489E D2	-4.84999E-02	-3.11984E-02	1.15183E 00	
160	-5.37127E-01	-4-65421E-01	4.6613QE 01	3.1488JE-04	4.934B9E 02	-4.35672E-02	-3.77839E-02	1-15 83E 00	
1 61	-4.65424E-01	-5.37125E-01	4-66130F 01	3.14883E-04	4.93489E 02	-3.774826-02	-4.359815-02	1.15183E 00	
162	-3.84245E-01	-5.97895E-01	4.66130E 01	3.14683E-04	4.93489E 02	-3.11619E-02	-4.85234E-02	1.15183E 00	
163	-2.952452-01	-6.46493E-0L	4-66130E 01	3.148835-04	4.93489E 02	-2-394256-02	-5.2460SE~Q2	1.15 83E 00	
164	-2.00234E-01	-6.41930E-01	4.6613QE 01	3.14883E-04	4.93489E Q2	-1.623696-02	-5.53304E-02	1-15183E 00	
165	-1.01148E-01	-7.03485E-01	4.66130E 01	3.14883E-04	4.93489E 02	-6.20179E-03	~5.70756E-02	1-15183E 00	
166	-4.73621E-06	-7.10720E-01	4-66130E 01	3-14883F-G4	4.93489E 02	-3.84039E-07	-5.76613F-02	1.15183E 00	
167	1.01142E-01	-7-03486E-01	4.6613QE 01	3.14883C-04	4.93489E 02	8.20130E-03	-5.7 07 57E-02	1.15183E QA	
168 169	2.092305-01	-6.81932E-01	10 30E188.4	3.14853E-Q4	4.93489E 02	1.62365E-02	-5.53305E-02	1-15183E 00	
170	2.95242E-01	-6.46494E-01	4.66130F DI	3.14883E-04	4.93489E 02	2.394226-02	-5.24606E-02	1-15167E 00	
171	3,84241E-01 4.65420E-01	-5,97696F-01	4.66130E 01	3.148836-04	4.93489E 02	3.11615E-02	-4-852366-92	1.15163E 00	
172	5.37125E-01	-5.37129E-01 -4.65424E-01	4.66130E 91 4.66130F 01	3.14883E-04	4.93489E 02	3.77479E-02	-4.359846-02	1.15183E 00	
173	5.97894E-01	-3.84246E-01		3-14883E-04	4.93489E 02	4.35670E-02	-3.7784ZE-02	1.15183F 00	
174	6,46492E-01	-2.95248E-91	4.66130E 01 4.66130E 71	3.14883E-04 3.14883E-04	4.93489E 02	4,84998E-02	-3.11986E-02	1.15183€ 00	
175	6.81930E-01	-2.00236F-01	4.66130E 01		4.93489E 02	5.24454E-02	-2.39757E-D2	1.15183E 00	
176	7.03485E-01	-1.01149E-01	4-60130F 01	3.14883E-04 3.14883E-04	4.93489E 02 4.93489E 02	5.53231E-02 5.70737E-02	~1.62619E-02	1-15183E 00	
177	8.12260E-01	0.0	4.33859E 01	2.971766-04	5.14420E 02	7.99593E-02	-8.21\$19E+93	1-15183E 90 1-20905E 00	
178	8.05855E-01	1.01803E-01	4-33850E 01	2.97176E-04	5.14420E 02	7.93274E-02	1-00426E-0Z	1.20705E 00	
179	7.86741E-01	2.02001E-01	4.33850E OL	2.97176E-04	5.14420E 02	7.744205-02	1.992492-02	1.20905E 00	
180	7-552206-01	2.99013E-01	4.33850E 01.	2.97176E-04	5-14420E 0Z	7.433356-02	2.94893E-02	1.20905E 00	
161	7.11789E-01	3.91309E-01	4.33850F 01	2-97176E-04	5.14420E 02	7.00514E-02	3.05038E-02	1.209050 00	
182	6.571322-01	4.77434E-01	4.3365Œ 01	2.971765-04	5.14420E 02	6.46645E-D2	4.706456-02	1.20905E 00	
183	5.92112E-01	5.56939E-01	4.33850E 01	2.97176E-04	5.14420E 02	5.82507E-02	5.47979E-02	1.209055 00	9
184	5.17754E-01	6-25857E-01	4.33850E 01	2497176E-04	5.14420E 02	5.09357E-02	6.16631E-02	1.20905E 00	
185	4.35231E-Q1	6.85813E-01	4.33850E 01	2-97176E-04	5.14420E 02	4.281186-02	6.755322-02	1.20905E 00	
186	3.458446-01	7.34954E-01	4.33850C 01	2.97176E-04	5-14420E 02	3.40154E-D2	7.23772E-02	1.20905E 00	
187	2.51003E-01	7.72505E-01	4.33850E 01	2,97176E-04	5-14420E 02	2.46851E-02	7,606126-02	1.20905E 00	
186	1.52203E-01	7-97872E-01	4.33850E 01	2-97176E-04	5.14420E 02	1.496766-02	7.854686-02	1.20905E 00	
189	5.10932E-02	5.10657E-01	4.3385QF, Q1	2.97176E-04	5.14420E D2	5.01545E-Q3	7.980ZZE-02	1-209056 00	
190	-5.100128-02	5.10657E-01	4.3385QE Q1	2.97176F-04	5.14420E 02	-5,015256-03	7.98022E-02	1.20905E 0D	
191	-1.52201E-01	7.97873E-01	4.3385QE 01	2.97176E-04	5.14420E 02	-1.49674E-02	7.85489£-82	1.20905E QO	
192	-2.51001E-01	7.72505F-01	4.33850E 01	2-97176E-04	5-14420E 02	-2,46849E-92	7.69612E+02	1.20965E 00	
193	-3.4 58 43E-01	7.34955E-01	4-3385 0 F 01	2.97176E-04	5.1442DE 02	-3.40152E-02	7.23773E-02	1.209055 90	
194	-4.35230E-01	6.85814E-01	4.3385QE 01	2.97176E-04	5.14420E 02	-4.28117E-02	6.75532E-02	1-20905E 00	
195	-5.17753E-01	6.25658E-01	4.33850E 01	2.97176E-04	5.1442DE 02	-5.09356E-02	6.166315-72	1.20905E 00	
196	-5.921;1E-01	5.56D31E-01	4.33850E 01	2.97176E-04	5.14420E 02	-5.82586E-02	5.47981E-02	1.20905E QQ	
197	-6.57131 2- 01	4.77436E-01	4.33850E Ol	2.97176E-04	5.14420E 02	-6,46644E-02	4.70647E-02	1.20905E 00	
198	-7.11788E-01	3.9131 0E -01	4.33850E 01	2.97176E-04	5.14420E 02	-7.00514E-02	3.55840E-02	1.20905E DO	
199	-7.55220E-01	2.99D14E-01	4.33850E 01	2.97176E-04	5.14420E Q2	-7.43334E-02	2.9485EE-02	1.20905E 00	
200	-7,86743E-Q1	2.02002E-01	4.33850E OL	2.97176E- 0 4	5.14420E Q2	-7.7442QE-02	1,992516-02	1.209058 00	

MD.	×	*	P	RHO	a	THETA	PEI		500Y
201	-8.05855E-01	1.01504E-01	4.338506 01	2.97175E-04	5.14420E 02	-7.93274E-02	1.0042EE-02	1-209 0 5E 00	
505	-A,12260E-Q1	1.284672-06	4.3345GE 01	2.97176E-04	5.14420E D2	-7.99593E-02	1.26734E-07	1.20905E 00	
503	-a. 05655E-01	-1.01802E-01	4.33850E 01	2.971766-04	5.1442DE 02	-7.93274E-02	-1.00425E-02	1.20905E 00	
204	-7.867426-01	~2.02000E-01	4.33850E D1	2.97176E-04	5.14420E 02	-7.7442 0E -02	-1.99248E-02	1.20905E 00	
205	-7.55221E-01	- 2.99012E-01	4.33450E 01	2.971762-04	5,14420E 02	-7.4333SE-02	-2 .94892 E- Q 2	1.20905E 00	
206	-7.117 9 02-01	-3.91307E-01	4.33 460 E 01	2.97176E-04	5.14420E 02	-7.00516E-02	~3 . 65# 37E~ Q2	1.20905E 00	
207	-6.57133E-01	-4.7743 <i>3</i> E-01	4.33 45QE 01	2.97176E-04	5_14420E 02	-6.46646E-02	-4,70644E-02	1-20905E GO	
208	-5.92113E-01	-5.56029E-01	4.3385QE 01	2.97176E-04	5.14420E 02	-6-82588E-02	-5.47976E-02	1.209055 00	
209	-5.17755E- 0 1	-6.25856E-01	4.33850E DI	2,97176E-04	5.14420E Q2	-6.09356E-02	-6-16630E-02	1-50302E #0	
210	-4.35232E-Q1	-6.85813E-01	4.33850E 01	2.971762-04	5.14420E 02	-4.26119E-02	-6.75531E-Q2	1.20905E 00	
211	-3.45845E-91	-7.34954E-01	4.338502 01	2.97176E-04	5.14429E 02	-3.401552-02	- 7. 237 726- 02	L.20905E DO	
212	-2.51004E-01	-7.7250 56- 01	4.3385 9 E 01	2-971766-04	5.1442 0E 0 2	-2.468512-02	-7.606 L ZE-02	1.209052 00	
213	-1.52205E-01	-7.97872E-01	4.33850E 01	2.97176E-04	5.14420E 02	-1.49677E-02	-7.85488E-02	1.20905E 00	
214	-5.10053E-02	-8.10657E-01	4.338506 01	2.97176E-04	5.14420E 02	-5.016666-03	-7.98021E-02	1.20 905£ 00	
215	5 .09983 E-02	-8.10657E-01	4,32850E 01	2.97176E-04	5.14420E 02	5.01497E-03	-7.96022E-02	1.20905E 00	
216	1.521986-01	-7,97873E-01	4.33850E 01	2.971765-04	5.14429E 02	1.496702-02	-7,55490E-02	1.209055 60	
217	2.50997E-01	-7.72507E-01	4.33850E 01	2-971762-04	5.14420E 02	2.46845E-02	-7.60614E-02	1.20905E 00	
218	3.45841E-01	-7.34956E-01	4.3385@E 01	2.97176E-04	5.14420E.02	3.401512-02	- 7.23773E-02	1.20905E 00	
219	4.35228E-01	-6.85815E-01	4.33850E 01	2.97176E-04	5.14420E D2	4.28115E-02	-6.79833E-02	1-209052 00	
220	5.177516~01	-6.25859E-01	4,33650E 01	2.971768-04	5,14420E 02	5.093542-02	-6,16633E-02	1.20905E 00	
521	5.921096-01	-5.56033E-01	4.33850E 01	2.97176E-04	5.1442GE D2	5.825646-02	-5.47983E-92	1,20905E 00	
222	6,571298-01	-4.77439E-01	4.3365GE 01	2.97176E-04	5.14420E 02	6.4664ZE-02	-4.70649E-02	1.20905E 00	
223	7-117876-01	-3.91312E-01	4.338506 01	2.97176E-04	5.14420E 02	7.00513E-02	-3.85841E-02	1-209056 00	
224	7.55219E-01	-2.990162-01	4.3385GE 01	2.971768-04	3.14420E 02	7.43334E-02	-2.94#96E-02	1.20905€ 00	
225	7.867406-61	-2.02005E-01	4.33850E 01	2.97176E-04	5.14420E 02	7.744196-02	-1.99253E-02	1.2090SE 00	
226	8.05654E-01	-1.01808E-01	4.33850E 01	2-97176E-04	5.14420E 02	7.932736-02	-1.00431E-02	1-20905€ 00	
227	0.13T40E-01	0.0	3,92450E 01	2.74067E-04	5.41875E OR	1-10491E-01	0.0	1.28600E 60	
225	9.08244E-01	1-005245-01	3,9245QE Q1	2.74087E-04	5.41675E 02	1.09728E-01	1,21940E-02	1.28699E 00 1.28699E 00	
230	8,91673E-01 5.64278E-01	1.99828E-01 2.96707E-01	3.92450E QL 3.92450E D1	2.74087E-04 2.74087E-04	5.41875E 02 5.41875E 02	1.07718E-01 1.04397E-01	2.42364E-02 3.59779E-02	1.28600€ 00	
231	8.26393E-01	3.89984E-01	3.92458E 01	2.74087E-04	5.41875E 02	9.98049E-02	4.72736E-02	1.28600E 00	
232	7.78476E-01	4.78527E-01	3.92450E 01	2.74087E-04	5.41875E 02	9.40002E-02	5.79E50E-02	1.28600E 00	
233	7.21109E-01	5.612612-01	3.92450E 01	2.74087E-04	5.41875E 02	6.70550E-02	6.79816E-02	1-28690E 00	
234	6.54989E-01	6.37182E-01	3. 9245 0E 01	2.74087E-04	5.41875E 02	7-905526-02	7,71431E-02	1.28600E 00	
235	5.00918E-01	7-95369E-01	3.92457E 01	Z.74087E-04	5.41875E G2	7.009945-02	5,53603E-02	1.28600E 00	
236	4.99796E-01	7.04994E-01	3. 92450E D1	2.74087E-04	5.41675E 02	6.02976E-02	9.25363E-02	1.28600E 00	
237	4.12607E-01	8.15332E-01	3.92450E 01	2.74087E-04	5.41875E 02	4.97692E-02	9.85872E+02	1.286 COE 00	
238	3.204102-01	8.55774E-01	3,92450E 01	2.74087E-04	5.41876E 02	3.06419E-02	1.034436-01	1.28600E 00	
239	2.24J23E-01	8+65828E-01	3,92450E OL	2.74087E-04	5,41875E 02	2.70502E-02	1.07049E-01	1.28600E 00	
240	1.25513E-01	9.05129E-01	3.92450E DI	2.740B7E-04	5.41875E 02	1.513396-02	1.09353E-01	1.28600E 00	
241	2.51796E-02	9.13443E-01	3.92450E 01	2.74987E-04	5.41875E 02	3.03595E-03	1.10359E-01	1.28600E 00	
242	-7.54595E-02	9-10669E-01	3,92450E 01	2.740B7E-04	5.41875E 02	-9.09536E-03	1.10027E-01	1.28600E 00	
243	-1.76183E-01	8.96841E-01	3.92450E 01	2.740B7E-04	5.41675E 02	-2.11236E-02	1.08369E-01	1.284000 00	
244	-2.727782-01	8.721265-01	3.92450E 91	2.74087E-24	5.41875E 02	-3.28982E-02	1.054056-01	1.28600E 00	
245	-3.67064E-Q1	8.34825E-01	3,924506 01	2.74087E-04	5.41075E G2	-4.42719E-02	1.01169E-01	1.286002 00	
246	-4,56894E-01	7.91366E-Q1	3.92450E 01	2.74087E-04	5.41875E 02	-5,511622-02	9.57072E-02	1.28600E 00	
247	-5.41178E-01	7.36301E-01	3.92450E 01	Z. 74087E-04	5.41875E 02	-6-52968E-02	5.90841E-72	1.25600E 00	
248	-6.188926-01	6.72298E-01	3.92450E D1	2.74087E-04	5.41875E 02	-7.46900E-02	8.13763E-02	1.28600E 00	
Z49	-6.89094E-01	6.00134E-01	3.92450E D1	2.74087E-04	5.41875E 02	-8.31809E-02	7.26740E+02	1.286QGE 00	
2 50	-7.50931E-01	5.20686E-01	3.92450E 01	2.74067E-04	5.418752 02	-9.06649E-02	6.398956-02	1.28600E 00	
						• • • • • • • • • • • • • • • • • • • •			

MACH 4 NOZZLE (G=1.24)

ZE = 2.05303E-01 STEP NO.

RHO THETA PSI BODY × Y HD. 2.74087E-04 -8.03653E-01 4.349176-01 3,92450E 01 5.41875E 02 -9-70498F-02 5.27109F-02 1.28600E 00 251 3.92450F 01 2.74087E-04 5.41875E 02 -1.02256E-01 4.169D6E-02 1.280000 00 252 -8.46620E-01 3.43869E-01 -1-06219E-01 3.015426-02 1-28600E 00 -0.79310E-01 2.48647E-01 3.92450E 01 2.74087E-04 5.41875E 02 253 1.50406E-01 -1.08689E-01 L.62438E-02 1.28600€ 00 -9.0132TE-01 3.92450E 01 2.740B7E-04 5.41875E 02 254 2.740B7E-04 -1-10233E-01 6.10667E-03 1.28600E 00 5.03401E-02 3.92450E 01 5.41 A75E 02 -9.12402E-01 255 -5.93372E-02 3.92450E 01 2.74087E-04 5.41875E 02 -1.10233E-01 -6.106326+03 1.28600E 00 256 -9-12403E-01 -9.01327E-01 -1.504032-01 3-92450E GL 2.74087E-04 5.41875E 02 -1-086895-01 -1.82434E-02 1.286006 00 257 5.41875E 02 -1.06219E-01 -3.01634E-02 1.28600E 00 258 -8.79311E-01 -2.48644E-01 J. 92450E 01 2.74007E-04 -1.022566-01 -4.16902E-02 1.286008 60 -3.43667E-01 3.92450€ 01 2.74087E-04 5.41879E 02 259 -8.466216-01 3.92450E 01 2.740872-04 5.41675E 02 -9.70580E-02 -5.2710SE-02 1.28600E 00 -8.03655E-01 -4.34914E-D1 260 3.92450E 01 2.74087E-04 5.41875E 02 -9.066528-02 -6.30802E-02 1.28600E 60 -7.50933E-01 -5.20683E-01 261 -6.00132E-01 2.74057E-04 -8.31611E-02 -7.26737E-02 1.28600E 00 -6.89096E-01 3.92459E 01 5.41875E 02 262 -6.18894E-01 -6.72296E-01 3.92450E 01 2.74067E-04 5-41875E 02 -7.46903E-02 -8.13760E-02 1.28600E 00 263 2.74087E-04 5-41879E 02 -6.52971E-02 -8.90639E-02 1.28600E 00 264 -5.4118DE-01 - 7**.** 36299E-01 3.92450E 01 -4.56896E-01 3-9245DE 01 2.74057E-04 5.41875E 02 -5.511652-02 -9.57570E-02 1.28600E 00 265 -7.91364E-01 -3.67057E-01 -8.36823E-01 3.92450E 01 2.74087E-04 5.41875E 02 -4.427236-02 -1.01 L68E-01 1.28600E DO 266 2.74087E-04 5.41875E D2 -3.28956E-02 -1.05405E+01 1.28000E 00 267 -2.72782E-01 -8.72125E-01 3.92450E D1 2.74087E-04 5.41875E 02 -2-11240E-02 -1.083692-71 1-25600E 00 -6.9684GE-01 3.92450E 01 266 -1.75186E-01 -7.54658E-02 -9.10068E-01 3.9245GE 01 2.74057E-04 5.41875E 02 -9.09914E-03 -1.10027E-01 1.28600E 00 269 1.28600E 00 Z70 2.51759E-02 -9.1344ZE-01 3.92450E 01 2.74087E-04 5.41875E D2 3,03849E-03 -1.10369E-01 1.28600E 00 2.74087E-04 5.41875E 02 1.51331E-02 -1.09363E-01 271 1.25507E-01 -9.05130E-01 3.92450F 01 3-92450E 01 2.74087E-04 5.41875E 02 2.78498E-02 -1.07849E-01 1.2860GE 00 2.24319E-01 - 6.45829E-01 272 1.28600E 00 -8.55776E-01 3.92450E 01 2.740072-04 5.418758 02 3.86412E-02 -1.03444E-01 273 3.20404E-01 1.28609E 00 -8.15334E-01 3.92450E OI 2.74DB7E-04 5.41875E QZ 4.97688E-02 -9.85874E-02 274 4-12604E-01 3.92450E 01 2.74087E-04 5.41875E 02 6.02970E-02 ~9.283665-02 1-28600E 00 275 4±9979 LE-01 -7.64997E-81 276 5.80916E-01 -7.05371E-01 3.92450E 01 2.74087E-04 5.41875E 02 7.00991E-02 -8,53605E-02 1.28600E 00 3.0245GE 01 2.740876-04 5.41875E D2 7.90347E-02 -7.71435E-02 1.28608E 60 277 6.54985E-01 -6.371 86E-01 7.21107E-01 -5.61263E-01 3.92450E 01 2.74087E-04 5.41875E 02 8.705476-02 -6.79618E-02 1.2860DE DD 278 7.75473E-01 -4.78531E-01 3.9245DE 01 2.74087E-04 5.41875E 02 9.39998E-02 -5,792552-02 1.28600E DD 279 3.92450E 01 2.74087E-04 5.41875E 02 9.980476-02 -4.72739E-02 1.28600E 00 280 9.26391E-01 -J.89986E-01 3.9245DE DI 2.74067E-04 5.41875E 02 1.04396E-01 -3.59785E-02 1.280000 00 261 8.64277E-01 -2.96712E-01 B.91672E-01 -1.99835E-01 3.92450E 01 2.74087E-04 5.41875E 02 1.077182-01 -2.42372E-02 1.28600€ 00 282 283 9-08243E-01 -1.005292-01 3.92450E OT 2.74087E-04 5.41875E 02 1.09728E-01 -1.21946E-92 1,286000 00 3.39530E 01 2.43870E-04 5.78388E 02 1.514625-01 1.392035 00 284 1.0153ZE 00 0.0 0.0 3.39530E 01 2.4387DE-04 5.7838BE 02 1.50703E-01 1.51959E-02 1.392036 00 265 1.01027E 00 1,01093E-01 3.3953QE 01 2.43870E-04 5.78388E 02 1.48436E-01 3.02340E-02 1.39203E 00 9,951898-01 2-011826-01 286 9.70212E-0 L 2.99271E-01 3.39530€ 01 2.43870E-04 5.78368E 62 1-44684E-01 4.49664E-02 1.39203E 00 287 9.35593E-01 3.94385E-61 3.39530E 01 2.436702-04 5.76368E Q2 1.39487E-01 5.92178E-02 1.39203E 00 TÉS 2 68 289 5.91676E-01 4.65580E-01 3.39530E 01 2.43870E-04 5.76388E Q2 1.329000-01 7.28670E-02 1.39203E 00 3.39530E 01 2.43870E-04 5.7838BE 02 1.2499 LE-01 8.57691E-02 1.39203# 00 YES 590 8.36897E-01 5.719502-01 1.39203E 00 TES 291 7.77750E-01 0.52635E-01 3.3953@E 01 2.43870E-04 5.78388E G2 1-156428-01 9.77962E-02 7.08934E-01 7.26833E-01 3.39530E 01 2.43870E-04 5.78386E 02 1.05548E-01 1.08832E-01 1.39203E 03 292 3.39530E 01 2.43870E-04 5.7838BE 02 9.42137E-02 L. L877GE-01 1.39203E 00 293 6.33642E-01 7.93899E-01 3.39530E 0t 2.43670E-04 5.78365E 02 8-195305-02 1.275186-01 1.39203E 80 294 5.50858E-01 6.52895E-01 4.03201E-01 9.03504E-D1 3.3953@E 6L 2.43870E-04 5.78386E 02 6.888926-02 1.34996E-01 1.39203E DO 295 296 3.70939E-01 9.45134E-Q1 3.39530E 01 2.43870E-04 5.78388E Q2 5.515206-02 1.41135E-01 1.39203E 00 2.43870E-04 4.08770E-02 1-458820-01 1.39203E 00 297 2.74991E-01 9.77371E-01 3.3953**0**E 01 5.78388E 02 2.620386-02 1.4919E-0L 1.39203E 00 298 1.76310E-Q1 9.99895E-01 3.3953**0E** 01 2.43870E-04 5.78388E 02 1.39203E DO 7.58759E-02 1.012465 00 3.3953Œ 01 2.43670E-04 5.78388E 02 1.12759E-02 1.510456-01 299 1.01500E 00 3.39530E 01 2.43870E-04 5.78386E 02 -3.76139E-03 1-514162-01 1.39203E DO YES 300 -2.53109E-02

MACH 4 NDZZLE (G=1+24)

NÙ.	×	₩	ρ	RHO	•	THETA	P\$[H	900Y
									u.e.e
301	-1.26247E-01	1.00744E 00	3.3953@C 01	2.43870E-04	5.78388E 02	-1.87623E-02	1.503042-01	1.39203E 07	YES
302	-2.25929E+01	9.898642-01	3.39530E 01	2.43870E-04	5.78388E 02	-3.35809E-02	1.47720E-D1 1.43686E-01	1.39203E 00 1.39203E 00	YES YES
303	-3.23364E-01	9.624500-01	3.395306 01	2-43870E-04	5.78388E 02	-4.80726E-02		1.39203E 00	YES
304	-4.17586E-01	9,2547[E-01	3, 39530E 01	2.43B70E-04	5.78388E 02	-6.20961E-02	1.38237E-01	1.39203E 00	YES
335	-5.07659E-01	8.79293E-01	3.39530E 01	2.43670E-04	5.78388E 02	-7.551326-02	1.31420E-01		
306	-5.92686E-01	8.24377E-01	3.39530E 01	2.43870E-04	5.78388E 02	-8-819142-02	1.2329@E-01	1.392032 00	YES
307	-6.71821E-01	7.61269E-01	3.39530E Ø1	2.43870E-04	5.78388E 02	-1.00004E-01	1.13944E-01	1.392036 00	YES
308	-7,44261E-01	6.97594E-01	3.39530E 01	2.438702-04	5.78388E 02	- L . 10832E-0 !	1.03445E-01	1.392036 00	YES YES
309	-B.09344E-01	6.13056E-01	3.39530E 01	2.43870E-04	5.78388£ 02	-1.20566E-01	9.18998E-82	1.J9203E 00	
310	-8.66362E-01	5.29425E-01	. 3.39530E 01	2,4387QE-04	5.783886 02	-1.29106E-01	7.941995-02	1.39203E 00	YES
31 I	-9.14771E-01	4.405322-01	3.39535E 01	2.43870E-04	5.78388E 02	-1.36363E-01	6.612778-02	1.39203E 00	AE2
312	-9.54068E-01	3,47261E-01	3.39530E 01	2.43870E-04	5.76388E 02	-1.42263E-01	5.215572-02	1.39203E 00	YES
313	-9.83923E-01	2.50540E-01	3.3953 0 E 01	2.43870E-04	5.78368E 02	-1.46744E-01	3.76453E-02	1.39203E 40	YES
314	-1.00398E 00	1.51327E-01	3.39530E 01	2.43870E-04	5.78388E 02	-1.49757E-01	2-2744E-02	1.39203E 00	YES
315	-1.01406E 00	5.061 LZE-02	3.39530E Ø1	2,43870E-04	5.78388E 02	-1.512726-01	7.608138-03	1.39203E 00	YES
316	-1.01406E 00	-5-06070E-02	3.39530E 01	2.43870E-04	5.7838BE 02	-1.51272E-01	-7.60750E-03	1.39203E 00	YES
317	-1-00398E 00	-1.51323E-01	3.395306 01	2.43870E-04	5.783BBE 02	-1.49757E-01	-2.27442E+02	1.3920JE 00	A E 2
318	-9.83924E-01	-2.50536E-01	3.39530£ 0l	2.43870E-04	5.783888 02	-1.46744E-01	-3.76447E-02	1-39203E 00	YES
319	-9.54089E-01	-3.47257E-01	3-395300 01	2.43870E-04	5.7838BE 02	-1.42264E-01	-5.21651E-02	1.39203E 00	YES
320	-9 -1 4773E-01	-4.43529E-01	3.39530E 01	2.43870E-34	5-78388£ Q2	-1.36364E-01	-6.612726-02	1.39203E 00	YES
321	-8.66364E-01	-1.29422E-01	3.39536E QL	2.43670E-04	1.78388E Q2	-1.29106E-01	-7.94154E-02	1+39203E 00	YES
322	-8.09346E-01	-6.13052E-01	3.39530E 01	2.43870E-04	5.78388E GZ	-1.20566E-01	-9.16993E-02	1.39203E 00	YES
323	-7.44284E-01	-6.90591E-01	3.3953QE 01	2.438702-04	5.783666 02	-1.10632E-01	-L.d3445E-01	1.39203E 00	ves
324	-6.71824£-01	-7.61260E-D1	3.39530E 01	2.43870E-04	5.78386E 02	-1.00004E-01	-1.139442-01	1.39203E 00	YES
325	-5.9268BE-01	-8.24376E-01	3.39530E 01	2.43870E-04	5,783886 02	-5.519172-02	-1.23295E-01	1.39203E 00	YES
326	-5.07662E-01	-8.79291E-01	3.3953 0 E 01	2.43879E-94	5.78J88£ 92	-7.55136E-02	-1.31420E-01	1.39203€ 00	YES
327	-4.17590E-01	-9.25469E-01	3.39530E 01	2.43870E-04	5.78388E 92	-6.20967E-02	-1.38236E-01	1.39203E 00	YES
326	-3.23366E-01	-9.62449E-01	3.3953 0 E 01	2.43870E-04	5.78388E 0 2	-4-80732E-02	-1.43686E-01	1.39203E 00	YES
329	-2 -25936E-01	-9.89862E-01	3.39530E 61	2.438708-04	5.78388E 02	-3.35827E-02	-1.47720E-01	1.39203E 00	YEŞ
330	-1.26254E-01	-1.00744E DO	10 30E20E.E	2.43870E-Q4	5.78388E 0 2	-1-416335-05	-1.50304E-01	1.39203E 00	YES
331	-2,5317 0E-0 2	-1.0150Œ DO	3.39520F 01	2.4387DE~D4	5.783B8E 02	-3.76229E-03	+1.51416E-01	1.39203E 00	YES
332	7.58717E-02	-1.01248E 00	3.3953DE 01	2.43870E-94	5.78388E 02	1.12753E-02	-1.51045E-01	1.39203E 00	YE5
333	1.76302E-01	-9.79696E-01	3.39530E 01	2,43870E-Q4	5.78388E 02	2,62026E-02	-1.49195E-01	1.39203E 00	YES
334	2.74984E-01	-9.77373E-01	3.39530E 01	2.436706-04	5.78388E 02	4.68760E-62	-1.45863E-01	1.39203E 00	YES
335	3.70934E-01	-9.451 J&E- 0 1	3.39530E dl	2.4387DE-04	5.78388E Q2	5.515132-02	-1.41136E-01	1.39203E 00	TĒS
336	4.63193E-01	-9-035086-01	3.39930E 01	2.438708-04	5.7838E Q2	6.88881 2- 02	-1.34996E-01	1.39203E 00	TES
337	5.50853E-01	-8.52898E-01	3.3953Œ 01	2.43870E-04	5.78388E 0 2	B.19522E-Q2	-1.275196-01	1.3 9 203E 00	YES
336	6.3303BE-01	- 7.93812E-01	3.39530E 01	2.43870E-04	5.78388E 02	9.42131E-02	-1,187705-91	1.392036 90	YE\$
339	7.08931E-01	- 7. 26536E-91	3.39 530E 0 1	2.43670E-04	5.78385E Q2	1.055482-01	-1.08832E-01	1.39203E 00	YES
340	7.77776E-01	- 6, 52640E-01	3.39530E <i>Q</i> 1	2.43870E-04	5.7836EE 02	1.15842E-01	-9.77970E-02	1.392032 00	YE\$
341	8.38893E-D1	-5.71955E-01	3.3953 0E 01	2.43870E-04	5.76388E 02	1-249902-01	-8.5769 8 E-02	1.39203E 09	YES
342	B.91674E-01	-4.85565E-91	3.39530E 01	2.43670E-04	5.7838BE 02	1.32900E-01	-7.28676E-32	1.39203E 00	YES
343	9.3559 0E~0 1	-3.94392E-01	3.39530€ 01	2.43870E-Q4	5.783866 02	1.39487E-Q1	-5,92188E-02	1.392 9 3E 00	YES
344	9.70210E-01	- 2, 99276E- Q 1	3.39530E 01	2.43B70E-04	5.7838BE 02	1-44684E-01	-4.49593E-02	1.39203E 00	YES
345	9.95188E-0 L	-2.71186E-01	3.39530E 71	2.43870E-04	5.78388E OZ	1.48436E-01	-3.02347E-02	1.39203€ 00	YES
346	1.01027E 00	-1.01097E-01	3.39530E #1	2.43870E-04	5.78388E 02	1.50703E-01	-1.51965E-02	1.392035 00	YES

MACH 4 NOZZLE (G=1.24)

BODY POINTS AT ZE = 2.05000E-01

STEP NO. B

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MO.	×	¥	P	RHO	o	THETA	PŠĪ	
284	1.01532E 00	0.0	3.39530E 91	2.43870E-04	5.7A388E 02	1.51462E-01	0.0	1.39203E 00
265	1.01027E QQ	1.01093E-01	3.39530E O1	2.438706-04	5.78388E 02	1.50703E-01	1.515596-02	1.39203E 00
286	9.951B9E-01	2.01182E-01	3.3953 0 E 01	2,43870E-Q4	5.78388E 02	1.48436E-01	J.QZ340E-02	1.39203E 00
267	9.7021ZE-01	2.99271E-Q1	3.39530E QL	2,438705-84	5.7838BE 02	1.44684E-01	4.49584E-72	1.39203E 00
265	9.35593E-01	7.94385E-01	3.39530E 01	2.43870E-04	5.7838BE 02	1.39487E-01	5.921782-02	1.39203E 00
2 6 9	8,91676E-01	4 .85580E-01	3.39530E 01	2.438706-04	5.783BAE 02	1.32900E-01	7.2867GE-02	1.39203E QO
290	5.38697E-01	5.71950E-01	3.39530E 01	2.43879E-04	5.75J88E 02	1 - 2499 LE-01	a_5769 LE-02	1.392036 09
291	7.7778 0E -01	6.55635E- 0 1	3.29530E 01	2.43870E-04	5.78388E 02	1-158426-01	9.77962E-02	1.392 63 E 00
292	7.08934E-01	7-26833E-01	3.29530E 01	2.43870E-04	5.78388E 02	1-05648E-01	1.0883ZE-01	1.39203E 00
293	6.37042E-01	7.93009E-01	3.3953 0E 0 1	2 • 4 3870E-04	5.78388E Q2	9.42137E-02	1.18770E-91	1,39253E 00
294	5.50858E-01	0.52895E-01	3.39530E 61	2.43870E-Q4	5.78388E 02	8,19530E-02	1-27518E-DL	1.39203E 00
295	4.63201E-01	9.03504E-01	3.39530E pi	2.43876E-04	5.78388E Q2	6.88892E-02	1.24996E-01	1.39203E 00
296	3.70939E-01	9,451 34E - 61	3.3953 0 E 01	2.43870£-04	5.78388E 02	. 5.51520E-Q2	1.41135E-01	1.39293E 99
297	2.74991E-01	9.77371E-01	3.3953 0 E OL	2,43570E-04	5.7638BE 02	4.08770E-02	1.456B2E-01	1.39203€ 00
298	1.763102-01	9.99895E-01	3,3953 0 E 01	2.43870E-04	9.78388E 92	2.62038E-02	1.49195E-01	1.39203E 00
299	7.58759E-02	1.01248E 00	3.39530E 01	2.43870E-04	5.783BBE 02	1.127596-02	l.51045E-91	1.39203E 00
300	-2.53109E-92	1.91590E 00	3.39530E 01	2.43870E-04	5.7838BE 02	-3.761392-03	1.51416E-01	1.392036 00
30 1	-1.262472-01	1.00744E 00	3.39530E D1	2.43870E-04	5.78308E 02	-1.8762JE-02	1.50304E-D1	1.39203E 00
302	-5.25989E-01	9.89864E-Q1	3.3953 0 E 01	2.43870E-04	5.7838BE 92	-J.35009E-02	1-47720E-01	1.392338 99
30.3	-3.23364E-01	9.62450E-01	3.39539E OL	2.43870E-04	5.78388£ Q2	~4,007262-02	1.436866-01	1.392 0 3E 00
304	-4.17586E-01	9.25471E-01	3.39530E 01	2.43870E-04	5.783882 02	-6,2096 JE-02	1-39237E-01	1.39203E 00
305	-5.07659E-01	8.79293E-01	3.39530E 01	2-43870E-04	5.7838BE 02	-7.551 32E-02	1.31420E-01	1.39203E 00
30 6	-5.92685E-01	8,2437 E-01	3,39536E 01	2 . 438 70 E- Q4	5.75388E 02	-6.81914E-02	1.23298E-01	1.39203E 00
307	-6.71821E-01	7.61269E-01	3,39530E 01	2-43B70E-04	5.76388E Q2	-1.00D04E-01	1.13944E-01	1.39203E 00
308	-7.44281E-01	6.905945-01	3.39530E 01	2.43B70C-04	5.78388E Q2	-1.10832E-01	1-03445F-01	1.39203E 00
30 0	-8.09344E-01	6.13056E-01	3.39530E 01	2-43870E-04	5.78388E Q2	-1.20566E-01	9.18598E-02	1.39203E 00
310	-8.66362F-01	5-29425E-01	3.39530E 01	2.43870E-04	5.78386E 02	-1.291 06E-01	7.94199E-02	1.39203E 00
311	-9.14771E-01	4.4063SE-01	3,3953 0 E 01	2.43870E-94	5.7838BE 02	-1.36363E-01	6.61277E-02	1.39203E 00
312	-9.5408E-01	3.47261E-01	3.39530E 01	2,43870E-04	5.78386E 02	-1-4226JE-01	5.21667E-02	1.392038 00
313	-9.83923E-01	2.50540E-01	3.39530E 01	2-43B70E-04	5,78388E 02	-1.46744E-01	3.764535-02	1.39203E 00
314	-1.00398E 00	1.51327E-01	3.3953 <i>0</i> E 01	2.438705-04	5.76388E Q2	-1.49757E-01	2.27448E-02	1.39203E 00
315	-1.01406F 00	5.061126-02	3.39539E 01	2.43870E-04	3.76388E 02	-1.51272E-01	7.608136-03	1.39203E 90
316	-1.01406E 00	-5,06070E-02	3.39530E 01	2-43670E-04	5.78388E 02	-1.51272E-01	-7.60750E-63	1.392 0 3E 00
317	-1.00398E 00	-1.513232-01	3.39530E 01	2.436705-04	5.78388E 02	-1.49757E-01	-2.27442E-02	1.392038 00
318	-9.83924E-01	-2.50536E-01	3.39530E 01	2.43870E-04	5.78388E QZ	-l.46744E-01	-3.76447E-02	1.39203E QQ
319	-9.54089E-01	-3.47257E-01	3.39530E 01	2.435702-04	5.78388E 02	-1.42264E-01	-5.21551E-02	1.392036 00
920 12E	-9.14773E-01 -8.66364E-01	-4.40529E-01	3.3953DE Q1	2.43870E-04	5.78388E 02	-1.36364E-01	-6.61272E-02	1.392036 00
		-5.294226-01	3.39530E Q1	Z.43870E-04	5.78388E 02	-1.29106E-01	-7.94194E-02	1.39203E QO
322	-8,09346E-01	-6.13052E-01	3.3953GE 01	2.438702-04	5.78388E 02	-1.20566E-01	-9.1899JE-02	1.39203E 00
323	-7.44284E-01	-6.90591E-01	3.39530E 01	2.43870E-04	5.78386E Q2	-1.108322-01	-1.03446E-01	1.39203E 00
324	-6.71824E-01	-7-61266E-01	3.3953QE 71	2.43870E-04	5.78386E 02	-1.009D4E-01	-1.13944E-01	1.39203E 00
325	-5.926562-01	-B. 24376E-01	3.30530E 01	2.43870E-04	5.78366E 02	-8.61917E-02	-1.23296E-01	1.39203E 00
326	-5.07662E-01	-8.79291E-01	3.3953GE DI	2,43870E-04	5.78366E 02	-7.55138E-02	-1.31420E-01	1.39203E 00
327	-4 . 1 7590E-01	-9.25469E-01	J.39530E 01	2.43870E-04	5.78360E 02	-6.20967E-02	-1.38236E-01	1.39203E 00
328 329	-3.23368E-01 -2.25936E-01	-9.62449E+01	3.39530E 01	2.43870E-04	5.78388E 02	-4.80732E-02	-1.43686E-01	1.39203E 00
330		-9.89862E-01	3.39530E 01	2.43870E-04	5.7838BE Q2	-3.35820E-02	-1.47720E-01	1.39203E DD
	-1.26254E-01	-1.00744E 00	3.39530E 01	2.43870E-04	5.783886 02	-1.87633E-02	-1.50304E-01	1-39203E 00
331	-2.53170E-02	-1.01500E 00	3.39530E 01	2.438702-04	5.78388E 02	-3.76229E-03	-1.51416E-Q1	1.392 03 € 00
332	7.5871TE-D2	-1.01248E 08	3.3953Œ .01	2.436706-04	5.783BBE 02	1.12753E-02	-1.51045E-01	1.39203E 00
333	1.76302E-01	-9.99896E-01	3.3953GE 01	2.43870E-04	5.78388E 02	2.620262-02	-1.49195E-01	1.39253E 00
334	2.74984E-01	-9.77373E-01	3.39530€ 01	2.43870E-04	5.78388E 02	4.08760E-02	-1.45883E-01	1.39203E 00
335	3.709346-01	-9.45136E-01	3.3953Œ 01	2-43870E-04	5.78368E 02	5.515134-02	-1-41136E-01	1.392036 00
336	4.63193E-01	-9.03508E-01	3,39530E Q1	R.43870E-04	5.78388F 08	6-88881E-02	-1.34996E-01	1.39203E 00

3

MACH & NOZZLE (G=1.24)

ZE = 2.40000E 01 STEP NO. 78

NO.	×	<u>_</u>	P	AHD	•	THETA	PŞI	M	BOOY
					1.08538E 03	2.34808E-03	6.37419E-04	4.96140E 00	•
1	7.151212-03	2.11067E-03	3.555886-01	6.16520E-06	1.08566E 03	-4.22301E-04	-1.59911E-05	4406453E 00	
2	4,49390E-01	-1.09172E-03	3.53214E-01	6.13894E-06				4.06516E 00	
3	2,21359E-01	3.73117E-01	3. 25 53 5E - 01.	6.13367E-06	1.08572F D3	-2.62734E-04	-2.81720E-73	4.06490E 00	
*	-2.19318E-01	3.79133E-01	3. 52 995E-01	6.13586E-06	1.08569E 03	2.10792E-03	-2.58816E-03	4.06612E 00	
5	-4.350;9E-01	2.36759E-03	3.522675+01	6.12567E-06	1.06580E 03	4.21596E-0J	4.12436E-04		
6	-2.11052E-01	-3.70560E-01	3.52267E-01	6.12567E-Q6	1-08580E 03	3.23143E-03	4.47893E-03	4.06612E 00 4.06577E 00	
7	2.26198E-01	-3.75347E-01	3.52474E-01	6.12857E-06	1.08577E 03	2.67819E-04	2.95320E-03	4.003776 00	
A	8.91646E-01	-1.95310E-03	3.30879E-01	5.82392L-06	1.88909E 03	-1.21533E-02	-3.60508E-04	4.10962E 00	
. 9	7.719708-01	4.537926-01	3,27348E-01	5.77375E-06	1.089656 03	-1.19936E-02	-7.17210E-03	4.1040ZE 00	
10	4.47107E-01	7.69488E-01	3.26105E-01	5.784520-06	1.0A953E 03	-7.23445E-03	-1.18913E-02	4,10859E 00	•
11	-9-97879E-04	8.84445E-01	3,27911E-01	5.78176E-06	1.08956E 03	-3.08736E-04	-1,5 4 555E-02		
12	-4.42445E-01	7.61 331E-01	3.29905E-01	5.81010E-06	1.08925E 03	6.493236-03	-1-29227E-02	4.10500E 0D	
13	-7.82699E-01	4.31777E-01	3.275BAE-01	5. 7771 4E-06	1.08961E 03	1.25721E-02	-8.54070E-03	4.10919E 00	
14	-8.853916-01	-1.36001E-02	3.28467E-01	5.78966E-06	1.08948E 03	1.43852E-02	-1.16577E-03	4.10759E 00	
15	-7.73187E-01	-4.571 01E-01	3-273712-01	5.77408E-06	1.08965E 03	1.35367E-02	7-21503E-03	4.10958E 00	
16	-4.39390E-01	-7.694 31E-01	3.27707E-01	3.77886E-06	1.05969E 93	7.64165E-03	1.33097E-02	4.10897E 00	
17	-8,67071E-03	-8.93179E-01	3,274836-01	5.77567E-06	1.08963E 03	9.19032E-05	1.61125E-02	4.10937E 00	
16	4,45141E-01	-7,73438E-01	3.29345E-01	5.80214E-06	1.08934E 03	-7.43061E-03	1.11815E-02	4.1060IE 00	
19	7 . 79180E - 0 1	-4.586412-01	3. 2761 4E -91	5.77754E-06	1.08961E 03	-1-17466E-02	6.37510E-03	4,10914E 08	
20	1.37393E 00	-6.02873E- 0 4	2.92100E-01	5.26691E-06	1.09550E 03	-3,43567E-Q2	-1.37679E-04	4.17747E 00	
21	1.30355E 00	4.43815E-01	2.89590E-01	5.230386-06	1-09594E D3	-3.30819E-02	-1.12236E-02	4.18263E 0C	
22	1.08626E 00	8.499382-01	2-89182E-71	5.22444E-06	1.09601E 03	-2.82813E-02	-2.04840E-02	4.18348E 00	
23	7.45380E-01	I.15798E 00	2.90500E-01	5.24363E-06	1.09578E 03	-1.89456E-02	-2.80995E-02	4.18076E 90	
24	J.30012E-01	1.33611E 00	2.89275E-01	5.22579E-06	1.095998 03	-0,46263E-03	-3.31 504E-02	4.18328E 09	
25	-1.24908E-81	1.36749E 90	2.90252E-01	5. 24003E-06	1.39582E Q3	2.10963E-03	-3.66229E-02	4.18127E 00	
26	-5.6522 8E-01	1.26215E 00	2.906 <i>8</i> 5E-01	5. 24633E-06	1.09575E 03	1 . 3921 5E- 62	-3.231316-02	4-180382 00	
· 27	-9.24966E-Q1	1.01912E 00	2.90505E-01	5.24457E-06	1.89577E 03	2 . 31 800E-02	-2.66016E-02	4,18052E 00	
28	-1.20933E 00	6-41014E-91	2.91375E-01	5.25637E-96	1.39563E 03	3.04957E-02	-1.83587E-02	4.17890£ 00	
29	-1.37389F 00	2.15042E-01	2.89631E-01	5.23098E-06	1.095932 03	3.32379E-02	-6.2144BE-03	4.18255E 00	
30	-1.37403E 00	-2.16651E-01	5 * 3002QE - 01	5.23708E-08	1.09586E Q 3	3.34291E-02	5.56077E-03	4,16168E 00	
31	-1.21708E 00	-6,4390GE-01	2.91072E-01	5. 251 96E-06	1.7956BE D3	3.07436E-02	1.72045E-02	4,17956E 00	
32	-9.30947E-01	-1-92529E 00	2.698326-01	5.23391E-06	1.095898 03	2,29946E-02	2.47825E-02	4.18713E OD	
33	-5.68897E-01	-1.26877E 00	2.69985E-01	5. 2361 4E-0B	1.09587E 03	1.36566E-02	3.106352-02	4.18182E 00	
34	-1.22385E-01	-1.37337E 00	2.90329E-01	5.24114E-06	1.39581F 03	1.68000E-03	3.55319E-02	4,1811LE 00	
36	3.33305E-01	-1.33783E 00	2.90150E-01	5. 23855E-06	1.09584E 03	-8.97205E-03	3.33066E-02	4,16148E 00	
36	7.45776E-01	-1.15874E 00	2.91331E-01	5.25572E-06	1.09563E 03	-1.90118E-02	2.77816E-02	4,17905E 00	
37	1.08695E QQ	-6.51287E-01	2.89637E-01	5,22961F-96	1-09595E 03	-2.62118E-92	2.006866-02	4.15274E 00	
38	1.30326E 00	-4.44846E-01	2.897526-01	5.23275E-06	1.09591E 03	-3.298752-02	1.0867 0 E-02	4.18230E 00	
39	1.91077E 00	-3.01963E- 04	2.65173E-01	4.87174E-06	1-10034E 03	-4.99822E-02	-1.72583E-04	4.235382 00	
40	1.64950E 00	4.67983E-01	2.64653E-01	4,86403E-06	1.130 44E 03	-4.83892E-92	-1.33620€-02	4.23657E 00	
41	1.66717E 00	9.10665E-01	2,64457E-01	4.86111E-06	1.10047E 03	-4.41712E-02	-2.45065E-02	4.23701E 00	
42	1.386L3E 00	1.29974E 00	2.65 09 2E-01	4.87053E-06	1.100352 03	-3.55529E-02	-3.37377E-02	4.23557E 00	
43	1.01865E 00	1.60685E 00	2.652626-01	4.87305E-06	1-10032E 03	-2.62437E+02	-4.18661E-92	4.23519E 00	
. 44	5-91087E-01	1.81100E 00	2.64978E-01	4.86BBSE-06	1-10038E 03	-1.57913E-02	-4.664036-02	4.23583E 00	
45	1.17238E-01	1.89194E DÔ	2.65057E-01	4.87001E-06	1-10036E 03	-5.30622E-03	-5.02086E-02	4.23565E 00	
46	-3.54398E-01	1.86833E 00	2.654628-01	4.87601E-06	1.170 <i>2</i> 9E 03	8.10364E-03	-4.91732E-02	4.23473E 90	
47	-8 - 16567E-01	1.73293E 00	2.64938E-01	4.86823E-06	1.100366 03	2.04404E-02	-4,44373E-02	4.23592E 00	
48	~1.21907E 00	1.47052E 00	2.651726-01	4.87172E-06	1.10034E 03	3 . l 37 29E-02	-3.868742-02	4.23539E 00	
49	-1.53399E 00	1.10439E 00	2.65821E-01	4.88133E-06	1.1002ZE 03	4.36003E-02	-3.014506-02	4.23392E 00	
50	-1.7697 8E 00	7.0131 <i>7</i> E-01	2.65806E-01	4.88119E-06	1.10022E 03	4.55838E-02	-1.76051E-02	4.23396E 00	
			•						

NO. P RHO a THETA 041 BODY -1-91144E 08 51 2.4352AE-0L 2.64780E-01 4.86591E-06 1.10041E 03 4.721126-02 -5.051492-03 4.23628E 00 52 -1.91022E 00 -2.42252E-01 2.65205E-01 4.87220E-06 1-190335 03 4.73993E-02 6.57225F-03 4-23531E 00 53 -1.7723LE OD -7.02293E-01 2.663458-01 4.88909E-06 1.10012E 03 4.54167E-02 1-88557E-02 4.23274E 00 54 -1.53612E 00 -1.10458E 00 2-66492F-01 4-89126E-06 1.10009E 03 3-96638E-02 3.07424E-02 4.23241E DO 55 -1.21983E OD -1-47235E 00 2.659798-01 4.883672-06 1.17019E 03 3.05011E-02 3.79037F-02 4-23356E 00 56 -8.15144F-0L -1-73403F 00 2-65615E-01 4.87628E-06 1.10026F 03 2.07655E-02 4.33870E-02 4.23439E 00 57 -3.54879E-01 -1.86891E 00 2-66297E-01 4.4883BE-06 1.10013E 03 9.37105E+63 4-78503E-02 4.23265F 00 58 1.20738E-01 -1.89337E DO 2-65942E-01 4.88312F-06 1.10020€ 03 -3.37556E-03 4.9823SE-02 4.23365E DO 59 5.92679E-01 -1.81334E 00 2.65778E-01 4.880695-06 1.10023E 03 -1-49617E-02 4.70571E-02 4.23402E 00 60 1.02051E 00 -1-60792E 04 2-658035-01 4.88107E-06 1.10022E 03 -2-58776E-02 4.17460E-02 4.23396E 00 61 1.38726E 00 -1.30085E 00 2.652398-01 4.87271E-06 1.10033E 03 -3.54546F+02 3-343116-02 4.23524E 00 62 1.66778E 00 -0.11297E-01 2-66616F-DI 4-86052E-06 1.10048E 03 -4.41680E-02 2-41376E-02 4.2371 GE 00 63 1.84924E 00 -4.68487E-01 2.646368-01 4.863776-06 1.10044E 03 -4.63951E-02 1.29875E-02 4.23661E 00 64 2.45512E 00 -5.43277E-05 2.55933E-01 4.734365-06 1.10209E 03 -5.19372E-02 -1.37360E-04 4.25670E 00 65 2.40397E 00 4.94343E-01 2.56987E-01 4.736668-06 1.10206E 03 -5.06619E-02 -1-14523E-02 4.25634E 00 66 2-247986 00 7.63433E-01 2-56048E-01 4.73609E-06 1.10206E 03 -4.79407E-02 -2-18619E-02 4.25643E 00 67 2-01151F 00 1.39257E 00 2.56247E-01 4-73904E-06 1.10203E 03 -4.08514E-02 -3.06176E-02 4.25596E 00 68 1.66779E 00 1.76726E 00 2-56787E-01 4.74710E-06 1.10192E 03 -3.42293E-02 -3.79159E-02 4.25469E 60 69 1.299126 00 2.07357E 00 2.56955E-01 4.74960E-06 1.10189E 03 -2.64444E-02 -4.50277E-02 4.25430E 00 70 8.54922E-01 2.28916E 60 2-573866-01 4.75603E-06 1.10181E 03 -1.69407E-02 -4.93717E-02 4.25329E 00 71 3.67935E-01 2.41757E 00 2.57179E-01 4.75294E-06 1-1018SE 03 -7.54789E-Q3 -5.21747E-02 4.253766 00 72 -1.14333E-01 2.45449E 00 2.57287E-01 4.754562-06 1-10163F D3 3.06675E-03 -5.04200E-02 4.25352E GD 73 -5.96842E-01 2.37259E 00 2.57112E-01 4.75195E-06 1.10166E 03 1.35197E-02 -4.95010E-02 4.25393E 00 74 -1.05641E 00 2.20393E 00 2.56902E-01 4.74881E-06 1.10190E 03 2.355972-02 -4.63632E-02 4.25443E 00 75 -1.48314E 00 1.93189E 00 2-570492-01 4.75100E-06 1.10187E 03 3.28665E-02 -4-16342E-02 4.2540BE 00 76 -1.86095E 00 1.58202E 00 4.75032E-06 2.57003E-01 1.10188E 03 4.003206-02 -3.349926-02 4.25419E 00 77 -2-14718E 00 1.1955GE 00 2.57224E-01 4.75361E-06 1.10164E 03 4-45080E-02 -2.33299E-02 4.25367E 00 78 -2.33705€ 00 7.47516E-01 2.56664E-01 4.74526E-06 1.10195E 03 4-8736BE-02 -1.39041E-02 4.25498E 00 79 -2.43832E DO 2.58743E-01 2.563606-01 4.74073E-06 1.10201E 03 5-13776F-02 -4.39443E-03 4.25570E Q0 80 -2.43460E 00 -2.60215E-01 2.565228-01 4.74314E-06 1.10197E 03 5.18135E-02 4.75748E-03 4.255328 00 81 ~2.33585E 00 -7.50766E-01 2.57001E-01 4.75029E-06 1.101862 03 4.89333E-02 1.47347E-02 4.25420E 00 82 -2.14591E 00 -1.20323E 00 2.5781 0E-01 4.76234E-06 1.10173E 03 4.41105E-02 2.40053E-02 4.25231E 00 -1.85948E 00 63 -1.58581E 00 2.57567E-01 4.758736-06 1-10177E 03 3.940736-02 3.37318E-02 4.23267E OD 84 -1.48250E 00 -1.93492E 00 2.57997E-01 4.765136-66 1.10169E 03 3.23337E-02 4.10820E-02 4.25187E 00 85 -L.06783E QQ -2.20772E OD 2.57676E-QL 4.76035E-GB 1.10175E 03 2.36212E-02 4.58252E-02 4.25262E QQ 86 -6.01614E-01 -2.37397E 00 2.578346-01 4.76279E-96 1-10172E 03 1-41613E-02 4.91118E-02 4.25225E 00 87 -1.16732E-01 -2.45115E 00 2.57946E-01 4.76438E-06 1.10170E 03 4.59947E-03 5.033616-02 4.251986 00 86 3.62460E-01 -2-42311E GO 2.57606E-01 4.75931E-06 1.10177E 03 -6.16844E-03 5.12618E-02 4.25276E 00 89 8.52137E-01 -2.28815E 00 2.57559E-01 4-75861E-06 1.10178E 03 -1.66605E-02 4.92900E-02 4.25289E DO 90 1.29879E 00 -2.07310E 00 2.56970E-01 4.749636-06 1-101892 03 -2.63965F-02 4.470126-02 4.25427E 00 91 1.68864E 00 -1.76820E 00 2.56629E-01 4.744 T4E-D6 1.10195E 03 -3.42464E-02 3.75997E-02 4.25506E 00 92 2.01262E 00 -1.39315E 00 2.560925-01 4.73674E-96 1-10206E 03 -4.09252E-02 3.033476-02 4.25632E 00 93 2.24874E 00 -9.63672E-01 2.5591 1E-01 4.73404E-06 1-10209E 03 -4.80036E-02 2.15704E-02 4.25675E 00 94 2.40399E 00 -4.94404E-01 2.56033E-01 4.73586E-06 1.10207E 03 -5.07000E-02 1.116756-02 4.25646E 00 95 2.99219E 00 -1.02171E-04 2.58047E-01 4.76587E-96 1-101688 03 -4.63557E-02 -1.04185E-04 4.25175E 00 96 2.95125E 00 4.96638E-01 2.583239-01 4.76998E-06 1.101636 03 -4.52393E-02 -8.28931E-03 4.25111E 00 97 2.83420E 00 9.79389E-01 2.58358E-01 4.770516-06 1-101622 03 -4.28231E-02 -1.59484E-02 4.25103E 00 98 2.63923E 00 1,41856E 00 2.58471E-01 4.77219E-06 1-10169E 03 -3.9898天 -02 -2.35£12E-02 4.25076E 00 99 2.34699E DO 1.83166E 00 2-55064E-01 4.76613E-06 1.10168E Q3 -3.61458E-02 -2.92669E-02 4.25171E 00 100 2-01923E 00 2-19701E 00 2.58773E-D1 4.77668E-06 1-10154E 03 -3.15846E-02 -3.40566E+02 4.25006E 00

MACH & MOZZLE (G=1.24)

ZE = 2.40000E DI STEP NO.

129 NO. RHO a THETA GODY 1.631426 00 2.57298E 00 4.7830GE-06 1-101466 93 -2.56352E-02 -3.69642E-02 4.24908E 00 101 2.59197E-01 4.24759E 00 102 1.19560E 00 2.7381 OE QQ 2.59839E-01 4.79254E-06 1.101346 03 -1.82757E-02 -4.23128E-02 103 7.34583E-01 2.69941E 00 2.59811E-01 4.79212E-06 1.10135E 03 -1-11491E-02 -4.49337E-02 4.24766E DO 104 2,603946-01 2.99566E 01 2.59712E-01 4.79066E-06 1.10137E 03 -2.75700E-03 -4.57713E-02 4-74788E 00 -2.50528E-01 2.97544E 00 2.59232E-01 4.78352E-06 1.10146E 03 J.62993E-03 -4.53302E-02 4.24897E 00 105 4.24889E 0D -7.36908E-01 2.89222E 00 2.59279E-01 4.78421E-06 1.10145E 03 1.051176-02 -4.51350E-D2 106 4.24795E 00 -1.20667E 00 2.73651E QQ 2.596861-01 4.7902BE-36 1.10137E 03 1.76396E-02 -4.236\$5E-02 107 4-24741E 00 -1.64108E 00 4.79372E-05 1.10133E 03 2.493656-02 -3.84367E-02 108 2.50400E 00 2.5991 BE-01 -2.007428 00 3-21249E-02 -3.38534E-02 4.24793E 00 109 2.19708E 00 2.59692E-D1 4.790366-06 1,101378 03 -2.15065E QQ 1.84217E 00 2.58905E-01 4.77866E-06 1.17152E 03 3.72530E-02 -2.77692E-02 4.24975E 00 110 4.24993E 00 111 -2.63492E 00 1.41409E 00 2.58829E-01 4.77732E-06 1.10153E 03 4.01884E~02 -2-2011 EE-02 4.24985E 00 -2.63581E 60 9.61306E-01 2.56665E-01 4.77805E-06 1.10153F 03 4.32083E-02 -1.5944BE-02 112 -2.95737E DO 4.81996E-01 1.101456 03 4.51838E-02 -8.67848E-33 4-24685E 00 113 2.59295E-01 4.78445E-05 -2.99178E 00 - 7.90806E-03 2.59652E-01 4.78976E-06 1.10138E 03 4.64739E-02 -8.24516E-04 4-24802E 00 114 4.24754E QD 115 -2.96069E 00 -4.86750E-01 2.59859E-01 4.79284E-05 1-10134E 03 4.485286-02 7.585536-03 116 -2.63334E 00 -9.65184E-01 2.59467E-01 4.78702E-05 1-1914IE 03 4.32196E-02 1.55877E-02 4.24845E 00 2.19070E-02 4-24623E 00 117 -2.63271E 00 -1.41863E DO 2.59566E-01 4.78848E-06 1.10139E 03 4.00352E-02 -2.35059E 00 -1.84615E 00 2.59599E-01 4.78898E-06 1.10139E 03 3.70132E-02 2.76434E-02 4.24615E 00 118 -2.00835E 00 -2.1990GE 00 2.60449E-01 4.80162E-05 1.10123E 03 3.18221E-02 3.35800E-02 4.2461BE 00 119 4-24561E 00 -1.64277E 00 -2.50524E 00 2.50596E-01 4.80529E-06 1.1011BE 03 2.48864E-02 3.784726-02 1 20 4.19701E-02 4.24642E 00 -1.20958E 00 -2.74011E DO 2.50344E-01 4.50006E-06 1-10125E 03 1.78203E-02 121 -7.38603E-Q1 -2.89463E 00 2.59922E-01 4.793786-06 1.10133E 03 1.09245E-02 4.52100E-02 4.24740E 00 122 123 -2.52325E-01 -2-97180E 00 2.59635E-01 4.78951E-06 1-10138E 03 4.10726E-03 4.59795E-02 4-24806E 00 4.24740E 60 124 2.56225E-01 -2,99339E 00 2.59920E-01 4.79376E-06 1.10133E 03 -2.44007E-03 4.455 DZE- DZ 4-24721E 00 125 7.29227E-D1 -2.89453E 00 2.60004E-01 4.79499E-06 1.101312 03 -1.07221E-02 4.44528E-72 1.19175E. DO -2.73584E 00 2.59731E-01 4.79094E-06 1-10136E 03 -1-82417E-02 4.24229E-02 4-24784E 00 126 1.62909E 00 -2.50339E 00 2.59101E-01 4.76156E-06 1.10148E 03 -2.56310E-02 3.88428E-02 4.24930E 00 127 -2.19948E 00 4-25050E GO 128 2.01829E 08 2.58585E-01 4.773BBE-06 1.10158E 03 -3.15871E-02 3.39175E-D2 1 29 2.34688E 00 -1.83327E CO 2.57881E-01 4.76340E-06 1.10171E 03 -3.61841E-02 2.91012E-02 4.25214E 00 4.25113E 00 130 2.63955E 00 -1.41959F 00 2.583120-01 4.76982E-06 1.10163E 03 -3.91407E-02 243370LE-02 131 2.83452E. 00 -9.79782E-01 2.58244E-01 4.76881 E-06 1.10165E 03 -4.28595E-02 1.57355E-02 4.25129E 00 132 2-95119E 00 -4.96853E-G1 2.58277E-01 4.769292-06 1-10164E 03 -4-52687E-02 8.07531E-03 4.251226 00 4.23253E 00 .133 3.51783€ 00 3.65123E-05 2.66439E-01 4.89048E-06 1.10010E 03 -3.70423E-02 -9.57351E-05 134 3.48026E 08 5.03517E-01 2.66583E-01 4.89262E-06 1.10005E 03 -3.63556E-02 -5.87225E-03 4.23220E QQ 135 3.37509E 00 9-984232-01 2.66566E-01 4-89236E-06 1.18008E 63 -3.45446E-01 -1 -09000E-02 4.23224E 00 136 3.20977E 00 1.4795AE 00 2.67365E-01 4.90418E-06 L-09993E 03 -3.17633E-02 -1.52266E-02 4.23045E DO 4.89693E-06 1.10002E 03 -3-15946E-02 -2.096362-02 4-23155E 00 137 2.94458E 00 1.90904E 00 2.66875E-01 2.30379 00 4.90394E-06 1.09994E 03 -2.6335QE-Q2 -2.47566E-02 4.23048E 00 1.36 2.657656 70 2.673492-01 2.30725E 00 2.65434E Q0 2-67770E-01 4.91017E-06 1.099862 03 -2.60933E-02 4-22954E 00 139 -2_43063E-02 140 1.40269E 00 2.95348E 00 2.67873E-01 4.91169E-06 1.09984E 83 -1.96343E-02 -3.15468E-02 4.22931E 00 141 1.46074E 06 3.19473E 00 2.68179E-01 4.91523E-06 1.09978E 63 ~1.44950E-02 -3.39117E-02 4.22862E 00 142 9.667676-01 3.37433E 08 2.68142E-01 4.91568E-06 1.09979E 03 -9.85764E-03 -3.52610E-02 4.22870E 00 4.95512E-Q1 3.49858E 00 4.92497E-06 -4.48553E-03 -3.50491E-02 4.22730E 00 143 2.68771E-01 1,09967E 03 144 -6.45288E-04 3.51440E 00 2.08789E-01 4.914892-06 1,09980E 03 9-431566-04 -3.72948E-02 4.22682E 00 -4.97104E-01 3-47886E QQ 2.68101E-01 4-91506E-06 1.099802 03 5.35749E-03 -3.67961E-02 4.22880E 00 145 4.22899E 00 146 -9-64251E-01 2.37313E 00 2.68014E-01 4.91378E-06 1.00081E 03 1.04179E-02 -34569335-02 1.517796-02 -3.30405E-02 4.22886E Q0 147 -1.45646E 00 3.201668 00 2.05071E-01 4.91463E-06 1.09980E 03 148 -1.90404E 00 2.96316E 00 2.66072E-01 4,91464E-06 1,099805 03 1.943386-02 -3.04093E-02 4.22886E 00 149 -2.30609E 00 2.65093E 00 2.67992E-01 4.91346E-06 1.09982E 03 2.35221E-02 -2.797296-02 4.22904E 00 4.22942E 00 1 50 -2.66105E 00 2.299258 00 2.67821E-01 4.910936-06 1.09985E 03 2.767852-02 -2.45705E-02

76

NO. × 8HD ۵ THETA -- 051 AAAV 2.67652E-01 4.90842E-D6 151 -2.95066F 00 1.89456E 00 1.09958E 03 3.18086E-02 -2.09756E-02 4-22980E 00 152 -3.20259E OD 1-46825E 00 2-67901E-01 4.91211F-06 1.09983E 03 3.33472E-02 -1.57709E-02 4-22924E 00 163 -3.37892F 00 1.00084E 00 2-67666F-01 4.90863F-06 1-09988E 03 3-50332E-02 -1-05434E-02 4.22977E 00 -3.48852E 00 5-061962-01 154 2.67643E-01 4.908295-06 1.09988E 63 3-58540E-02 -5.08993E-03 4.22982E 88 155 -3.51996E 00 1.64540E-03 2.676225-01 4.90798E-06 1.09986E 63 3-05005E-02 -3-27533E-05 4-22987E 60 -3.49313E 00 -5.09308E-01 156 2.67922E-01 4.91243E-06 1.099836 03 3-491286-02 4-83723E-03 4.22920E 00 -3.37626E 00 157 -1-00477F 00 2.67945E-01 4-91276F-06 1.09982E 03 3.454576-02 1-02625E-02 4-229155 00 158 -3-19962E 00 -1.47115E 00 2-68392E-01 4-91937E-06 1.099746 03 3-30402E-02 1.567316-02 4-22614E 00 159 -2.95066E 00 -1.8979IE 00 2.68231E-01 4.91699E-06 1.39977# 03 3.15049E-02 2.08762E-02 4-22651E 00 160 -2-66214E 00 -2.30267E 00 2.68479E-01 4.920655-06 1.09973E 03 2-73474E-02 2.44485E-02 4-22795E 00 161 -2.30723E 00 -2.653036 00 2.68709E-01 4.92399E-06 1.09968E 03 2-322075+02 4-22745E GG 2.77889E-02 16± -1.90598E 00 -2.96385E 00 2.68813E-01 4.92559E-06 1.09966E 03 1-9197DE-02 3.01228E-02 4-22721E 00 163 -1-45887E 00 -3,20242E 00 2.68733E-01 4.92441E-06 1.09968E 03 1-501316-02 3.27905E-02 4.22739E 00 164 -9-83608E-01 -3.37482E 00 2.68774E-01 4.92501 E-06 1.09967E 03 1-01960E-02 3.54674E-02 4.22729E 00 165 -4 -98253E-01 -3.48634E 50 2.68932E-01 4.92736E-06 1.09964E 03 4.46887E-03 3-65437E-02 4.22694E 08 -1.76545E-02 -3.51548E 00 166 2.6851 0E-01 4-921126-06 1-099728 03 -9-63455E-04 3.727556-02 4-22788E 00 167 4.96384E-01 -3.49185E 00 2.68435E-01 4.92001E-06 1.09973E 63 -5.02267E-03 3.51213E-02 4.22805E 00 168 9.847268-01 -3.37029E 00 2.67984E-01 4.91334E-06 1.099826 03 -9-88378E-03 4.22986E 00 3.519395-02 169 1.45685E 00 -3.19509E 00 2.67919E-01 4.91238E-06 1.09983E 03 -1.46873E-02 3-39810E-02 4.22920E 00 170 1-899735 00 -2.95531E 00 2.676330-01 4.90815E-06 1.09988E 03 -1.98023E-02 3.139296-62 4.22984E 00 171 2.305426 60 -2.65619E 00 2-67452E-01 4.90546E-06 1.00002E 03 4.230256 00 -2.44397E-02 2.79268E-02 172 2.65666E 00 -2.30485E 00 2.67046E-01 4.69949E-06 1.00000 63 -2.84575E-02 2.45582E-02 4-23116E 00 173 2.94436E 00 -1.90974E DO 2.666325-01 4.093346-06 1.10007E 03 -3-16647E-02 2.07467E-02 4.23209E 00 174 3.20997E 00 -1.47975E 00 2.671 B7E-01 4.90154E-06 1-09997E 03 -3.18296E-02 1.50192F-02 4.23085E 00 175 3.37931E OD -9.98357E-01 2.66468E-01 4-890916-06 1-100106 03 -3-45889E-02 1.06857E-02 4.23246E 00 176 3-48030E 00 -5.03418E-01 2.66545E-01 4.89205E-05 1.1000BE 03 -3.63861E-02 5.67E86E-03 4-23229E DO 177 4.0288E 00 -7.55741E-D5 2.782 BBE-01 5.0651 42-08 1.09794E 03 -2.56541E-02 -7.36153E-05 4.20644E 00 178 3.99537E 00 5.06424E-01 5.06590E-06 4.20633E DO 2.78341E-01 1.09793E 03 -2.54401E-02 -3-66967E-03 . 179 3.89889E 00 1.00269E DO 2.78255E-01 5.06465E-06 1.09794E 03 -2-473262-02 -7.09233E-03 4-206522 00 180 7.74375E 00 1.48774E DO 2.786595-01 5.07058E-06 1.09787E 03 -2.33712E-02 -9.35900E-03 4.20565E 00 181 3.52134E Q0 1.96348E 00 2.79091E-01 5.07691E-06 1-09779E 03 -2.29264E-02 -1-11563E-02 4.20472E 00 152 3.26940E DD 2.379372 00 2.796182-01 5.084646-06 1.09770E 03 -2.06093E-02 4.203596 00 -1-45265E-02 183 2-94603E 00 2.75919E 00 2.79695E-01 5.06578E-06 1-09769E 03 -1.84672E-02 -1.752236-02 4.20343E Q0 184 2.570 20E 00 3.099DOE 00 2.79640E-01 5.08497E-06 1.09770E 03 -1.60580E-02 -L.99323E-02 4.20354E 00 185 2.15682E 00 3.39370E 00 2.79676E-01 5.08550E-06 -1.316846-02 1.09769E 03 -2.22775E-02 4.20347E 00 1-71666E QQ 186 3.633386 90 2.79787E-01 5.08712E-06 1.09767E 03 -1.01575E-02 -2.43966E-02 4.20323E 00 1.24233E 00 3.81231E 00 167 2.79459E-01 5.08231E-06 1.09773E 03 -7.63105E-03 -2.60273E-02 4-20393E 00 188 7-43042E-01 3.96175E 00 2.80275E-01 5.09427E-06 1.09758E 03 -4.75281E-03 -2.442746-02 4.202198 00 189 2.35788E-01 4.03754E 00 2.80580E-01 5.09846E-06 1.09753E 03 -2.02516E-03 -2.41407E-02 4.2015BE 00 190 -2-50399E-01 4.03199E 00 5.098852-06 2.50587F-01 1.09753E 03 1-94884E-03 -2.526756-02 4.20152E 00 191 -7.46426E-01 3.96091E 00 2.80377E-01 5.09577E-06 1.09756E 03 5-13914E-03 -2.46869E-02 4.20197E 00 192 -1.23376E 00 3.831588 00 2.80054E-01 5.09103E-06 1.097626 03 8.59006E-03 -2.41B98E-02 4.20266E 00 193 ~1.70206E 00 3.64652E 90 2.79931E-01 5.48924E-26 1.09764E 03 1.17779E-02 -2.301282-02 4.202926 00 194 -2.14644E 00 3.39678E DO 2.79638C-01 5.064946-08 1.097706 03 1-45513E-02 -2.24007E-02 4.20355E DO 195 -2.56357E 00 3.08726E 00 2.79536F-01 5.0834SE-06 1-097716 03 1.64105E-02 -2.11722E-02 4.20377E 00 -2.94761E 00 2.74857E 00 2.79790E-01 196 5.257165-06 1.39767E 03 1.759746-02 -1-81990E-05 4.20322E 00 197 -3.26959E 00 2.36444E 00 2.80044E-01 5.09089E-06 1.09762E 03 1.999958-02 -1.52443E-02 4.2026BE 00 -3.53523E 00 196 1.95744E 00 2.80123E-01 5-09204E-06 1.09761E 03 2.20689E-08 -1-159256-02 4.20251E 00 199 -3.74860E 00 1.50191E DO 2.79787E-01 5-097128-96 1-09767E 03 2.J3266E-02 -8.332106-03 4.20323E 00 200 -3.90128E 00 1.01776E 00 2.79372E-01 5.08103E-06 1-09774E 03

2.47124E-02

-8-14711E-03

4-20412E DO

MACH 4 NDZZLE (G=1.24)

ZE = 2.40000E DI . STEP NO. 78

NO.	x	٧	P	RHO	a ,	THETA	PST	M	ROOY
20 1	-3.99521E 00	5.1868 9 E-01	2.79269E-01	5.07953E-06	1.09776E 03	2.58137E-02	-1.95856E-03	4,204345 00	
202	-4.01394E 00	6.13514E-93	2.789455-01	5.37477E-06	1.09782E 03	2.72975E-02	7.05304E-04	4.20503E 00	
203	-3.99110F 00	-5.16968E-01	2.7931 9E-01	5.08026E-06	1.09775E 03	2.56B74E-02	2.76967E-03	4.20423E 00	
204	-3.89769E 00	-1.022446 00	2.79491F-01	5.08279E-06	1.09772E 03	2-451196-02	5.30549E-03	4.29386E 00	
20 5	-3.74739E 00	-1.50431E D7	2.80236E-01	5,09371 E-06	1-79759E 03	2.30479E-02	8.26729E-03	4.20227E 00	
296	-3.53577E 00	-1.95850E QO	2.806875-01	5,100325-06	1.09751E 03	2.165686-02	1.149356-02	4.2013QE 00	
207	-3.27100E QO	-2.365 63 E 00	2.80676E-01	5.10016E-06	1.B9751E 03	1.982446-02	1.512386-02	4.20133E 00	
208	-2.94910E 00	-2.75048E 90	2.804566-01	5.99693E-06	1.09755E 03	1.74402E-02	1.803256-02	4.2018QE 00	
200	-2.56495E 00	-3.08879E 00	2.802QJE-01	5.09322E-06	1.09759E 03	1.629466-02	2.096726-02	4.20234E 00	
210	-2.14830E 00	-3.39751E 00	2-802514-01	5.09393E-06	1.09759E 03	1.450696-02	2-214006-02	4.202248 00	
211	-1.70388E 00	-3.645586 00	2.80390F-01	5.09596E-06	1.09756E 03	1 - 1 86 85E-0 2	2.28560E-02	4.20194E 00	
212	-1.23364E 00	-3.82720E 90	2.80395E-01	5.09604E-08	1.09756E 93	8.787756-03	2,40135E-02	4.20193E 00	
213	-7.45312E-01	-3.962542 00	2.80717E-01	5.10076E-06	1.0975QE 03	5.08756E-03	2.39875E-02	4.20124E 00	
214	-2.47285E-01	-4.045226 79	2.8128SE-91	5.10907E-06	1.09740E 03	1.600186-03	2.40995E-02	4-20003E 00	
215	2.41859E-Q1	-4.02364E 00	2-80246E-01	5.093856-06	1.097596 03	-2.25026E-03	2,54520E-02	4.202256 00	
216	7.44533E-01	-2.96337E 00	2.80259E-01	5.094 Q4E-06	1.097586 03	-4.83986E-03	2.48280E-02	4.20222E 00	
217	1-23889E 00	-3.81510E 00	2.794125-01	5.081626-06	1.99774E D3	-7.55354E-Q3	2.5924CE-02	4.20403E 00	
218	1.71201E 00	-3.63581E 00	2.79519F-01	5.08319E-06	1-09772E 03	-1.027796-02	2.440456-02	4.20380E 00	
219	2.15531E 60	-3.39532E 00	2.79391E-01	5.081312-06	1.09774E 03	-1.33319E-02	2.21900E-02	4.20408E 00	
220	2.56781E 0D	-3.10058E 00	2.79287E-01	5,179796-06	1-09776E 03	-1.62362E-02	1 - 98 : 28E-02	4.20430E 00	
221	2-94444E 00	-2.76045E 90	2.79362E-01	5.08D88E-06	1.09775E 03	-1.6609ZE-02	1.737216-02	4.20414E 00	
222	3.26840E 00	-2.380596 AG	2.79323E-01	5.08034E-06	1.09775E 03	-2.07269E-02	1.43563E-02	4.204226 00	
223	3.52088E 00	-1.96428E 00	2.76870E-01	5.07368E-05	1.39783E 03	-2.301275-02	1-099236-02	4.20519E 00	
224	3.74380E 00	-1.48824E 00	2.78513E-01	5.06844E-06	1.097902 03	-2.34259E-02	9-18410E-03	4.20596E 00	
225	3.69911E 00	-1.00Z90£ DO	2.78181E-01	5.06356E-06	1.09796E 03	-2-47679E-02	6.91311E-03	4.2066BE 00	
220	3.99541E 00	-5.06569E-01	2.7831 0E-01	5.06545E-06	1.09793E 03	-2.54618E-02	3.71113E-03	4.20640E 00	
227	4.51574E 00	-3,27531€-05	2.91368E-01	5.256272-06	1.09563E 03	-1-313126-02	-6.61178E-05	4.178976 90	
228	4.4879ZE 00	4.98631E-01	2.91430E-01	5.25716E-06	1.09362E 03	-1.31084E-02	-1.78845E-03	4-17885E 00	
229	4.40551E 00	9.89509E-01	2-91440E-01	5.25732E-Q6	1.095615 03	-1.30100E-D2	-3,419426-93	4.178826 02	
230	4.27150E 30	1.469682 00	2.91797E-01	5.26251E-06	1.09555E 63	-1.250266-02	-4.48567E-03	4.17809E 00	
231	4.07409E 00	1-9246BE 00	2-912965-01	5.25522E-06	1.09564E 03	-1.26719E-02	-5.78140E-03	4.17912E 00	
232	3-86229E 00	2.37699E 00	2.9286 GE - GL	5.27796E-06	1.09537E 03	-1.01000E-02	-6.13075E-03	4.17592E 00	
233	3.566300 00	2.78865E 00	2.92542E-01	5.273346-06	1.09542E 03	-1.01551E-02	-7.36140E-03	4.176576 00	
234	3.22717E 00	3.15986E 00	2.925256-01	5.274545-06	1-09541E 03	-9.852886-03	-8.85971E-03	4.17640E 00	
235	2.85680E 00	3.49222E 00	2.92736E-01	5.2761BE-05	1.09539E 03	-8.905362-03	-9.91115E-03	4.17617E 00	
236	2.45807E 00	3.78437E 00	2.93311E-01	5.280162-06	1.09534E 03	-7.55377E-03	-1.09266E-02	4.17561E 00	
237	2.03070E DO	4.03065E 00	2.93330E-01	5.28479E-06	1.09529E 63	-6.12232E-03	-1.20606E-02	4.17497E 00	
238	1.577985 00	4.221326 00	2.93223E-01	5.28324E-06	1.095312 03	-4.552922-03	-1.37006E-02	4.17516E 00	
239	1-11792E 00	4.36735E QQ	2.93247E-01	5.28359E-05	1-99530E 03	-2.29803E-03	-L.38473E-02	4-17513E 00	
240	6.35944E-DI	4.474892 00	2-93460E-01	5.28668E-06	1.09526E 03	-7.771762-04	-1.26541E-02	4.1747GE 00	
241	1.310485-01	4.53384E 00	2.93841E-01	5.29222E-06	1.095202 03	-2.71609E-04	-1.16703E-02	4.17392E 00	
242	-3.79793E-01	4.50089E DQ	2.93140E-31	5.28202E-06	1.09532E 03	7.907752-04	-1.31671E-02	4-17535E 00	1
243	-8.75543E-01	4.42666E 00	2.93231€-01	5.28336E-06	1.09230E.03	1-979898-03	-1.30485E-02	4.17516E 00	
244	-1.35607E 00	4.30368E 00	2.93179E-01	5.28260E-06	(1.09531E 03	3.277148-03	-1.28535E-D2	4-17527E 00	
245	-1.82017E 00	4.13166E 00	2.93378E-01	5.285496-06	1.09528E 03	4.72764E-03	-1.247736-02	4.17487E 00	
246	-2.26046E 00	3.90395E 00	2.93281E-01	5.28408E-06	1.09530E 03	6.58562E-03	-1.24913E-02	4-17507E 00	
247	-2.66709E 00	3.63462E 00	2.93062E-01	5.28090E-06	1.09533E 03	5.61640E-03	-1.15158E-02	4.17551E 00	
24B	-1.03985E 00	3.32806€ 00	2.92993E-01	5.27989E-06	1.09535E 03	9.974298-03	-9.68444E-03	4,17565E 00	
249	-3.39711E 00	2.98290E 00	2.93048E-01	5.28069E-06	1.09534E 03	9.00809E-03	-7.72090E-03	4.17554E 00	
250	-3-71118E 00	2.58792E 00	2.93000E-01	5.279496-06	1-09534E 03	1.030516-02	-6.783685-03	4.17564E DO	
				-47 90	1 -4 - D 7 - C A D	. 10 20 22 - 42			

MACH 4 MOZZLE (G=1.24)

ZE = 2.40000E 01 STEP NO. 1

ND.	x	Y	P ·	RHD	Q	THETA	PSI	M	BODY
251	-3,97710E 00	2.15 395E 00	2-92827E-01	5.27748E-06	1.09537E 03	1.108865-02	-5.92400E-03	4.17599E DO	
252	-4.18996E 00	1.695 1E 00	2.92712E-01	5.27581E-06	1-09539E 03	1.164Z6E-02	-5.20449E-03	4.17623E 00	
263	-4.34927E DO	1.22017E 00	2,92573E-01	5.273762-06	1.09542E 03	1.22537E+02	-4.23742E-03	4.17651E 00	
254	-4.45868E 70	7.33235E-01	2.92796E-D1	5.27706E- 0 6	1-095J8E 03	1,28476E-02	-2,92104E-03	4.176058 00	
255	-4.50435E 00	2.38035E-01	2. 9250 0E -01	5.27709E-06	1.095386 03	L.42871E-0Z	~1.1956IE-03	4.17605E DQ	
2 56	-4.50150E 00	-2.44419E-01	2.9261 <i>8</i> E-01	5.27444E-06	1.095418 03	1.44612E-02	1.5344GE-03	4.17642E DO	
257	-4.45331E 00	-7.34110E-0L	2.92862E-01	5.27799E-06	1.09537E 03	1.3222 8E-Q2	3.32249E-03	4.1759?E DO	
258	-4.34923E 00	-1.22111E 00	2.92791E-01	5,27695E -9 6	1-09536E 03	1.225635~02	4.50955E-D3	4.17607E Q0	
259	-4.19096E DD	-1.69559E @B	2.93123E-01	5-281 76E-96	1.09532E 03	.1.14032E-02	5.322246-03	4.17539E 00	
260	-34978D4E 00	-2.15414E 00	2.93332F <i>-</i> 01	5.20481E-06 .	1.095292 03	1.09068E-02	6.00307E-03	4.17496E 00	
261	-3.71191E 00	-2.58829E 00	2.935765-01	5.28836E-06	1.09524E 03	1.01941E-02	6.764G8E-03	4.17446E 00	
262	-3.39758E 00	-2.98383E 90	2.93666E-01	5.28968E-06	1.09523E 03	9.79480E-03	7,66897E-03	4.17428E 00	
263	-3.040012 00	-3.3295 <i>6</i> E 0 0	2.93658E-01	5. 28956E-06.	L.09523E 03	9.91250E-03	9.61209E-03	4.1743 0 E D0	
264	-2.66598E 00	-3.63651E 00	2.93715E-01	5. 2903BE-06	1.09522E 03	8.58098E-03	1.14091E-02	4,17418E 00	
265	-2.26003E DQ	-3.90575E 00	2.93897E-01	5.293036-06	1.09519£ 03	6.57630E- 03	1.23680E-02	4,17381E DO	
266	-1.81940F 00	-4.1319JE 00	5.626166-01	5 • 29335E-94	1-09519E Q3	4;75424E-QJ	1,24825E-72	4.17377E 00	
267	-1.35614E 00	-4.29992E 00	2.93593E-01	5.26862 <i>F-</i> 06	1.09524E 03	3.30661E~03	1.29538E-02	4.17443E DO	
2 68	-8.79377F-01	-4.42318E OD	2.934896-01	5.28710E-06	1.09526E 03	2.00598E- 03	1.2685JE-02	4.17464E DO	
269	-3.81739E-01	-4.50984E 00	2.9379年-01	5.29155E- 9 6	1.09521E 03	1.352776-03	1.29586E-02	4.1740ZE QQ	
270	\.J?555E-Q1	-4.325SG 00	2.93682E-01	5.28991E-D6	1.09523E 03	5,1824BE- 04	1.25573E-02	4.17425E 00	
271	6.31691E-01	-4.47729E BO	2.93480E-01	5.286976-06	1.09526E D3	-7.003046-04	1.29140E-02	4.17466E QQ	
272	1.11586F 00	-4.3710SE 00	2.93140E-01	5.2820JE-06	1.3953ZE 03	-2,30097E-03	1.374845-02	4.17535E 00	
273	1.57635E QQ	-4.22247E 00	2.93024E-01	5.28035E-06	1.09534E 03	-4.58646E-D3	1.356196-02	4.17559E 00	
274	2.02837E 00	-4403047E DD	2.92938E-01	5.279106-06	1.09535E 0 3	-6,24937E-03	1.205765-02	4.17576E 00	
275	2.4560 <i>T</i> E 00	-3.78435E QO	2 .92653E-01	5,274956-06	1.09540E 03	-7.72036E -03	1.08712E-02	4,17635E QQ)
276	2.85533E 00	-J.49272E 00	2,923 54E-0 1	5.27061 E-08	1.095466 03	-9,67215E-03	9.8 29 00E-03	4,17696E QQ)
277	3.22615E 00	-3.16048E 00	2,92273E-01	5.269416-00	1.09547E D3	-1.00166E-D2	6.7207Œ-03	4.17712E 00	•
278	3.56555F 00	-2.76941E 00	2.92216E-01	5.26860E-06	1.09548E DJ	-1.02996E-02	7.18955E-03	4.17724E 00	
279	3.8616DE 00	-2.37751E 00	2.92581E-01	5.2739 E-06	1.09542E 03	-1.02807E-02	5-96727E-03	4,17649E 00)
250	4.07385E DD	-1.92509E 06	2.91099E-01	5.252358+06	1.09567E 03	-1,27449E-02	5.620842-03	4.17953E 00	
28 1	4.27152E 00.	-1.46988E QO	2.91671E-01	5.26967E-06	1-09557E 03	-1.25543E-02	4.31322E-93	4.17835E 03	
262	4,40569E 00	-9.89533E-Q1	2.91371E-D1	5. 25632 E-06	1.09563E 03	-1.30401E-02	3.250892-03	4.17897E 00)
283	4.48803E 00	-4.98666E-01	2.91 399E -01	5.29672E-06	1-09562E 0 3	-1.31215E- 0 2	1-64480E-03	4.17891E 00	
284	4.97253E 00	- 8.13480E-05	J.03216E-01	5.42	1.09360E 03	-3,52451E-04	-5.72648E-05	4.15519E QQ	YES
285	4,94794F 00	4.94179E-01	3.9328ØE-01	5. 4290 1 E-06	1.09359E D3	-3.32952E-04	-2.10671E-04	4.15504E 00	
286	4-87441E 00	9.83409E-01	3.03378E-01	5.43030E-06	1.09357E 03	-2.84692E-04	-3.6752JE-04	4-15487E 00	
287	4.752076 00	1.465 0 4E DQ	3.0343 <i>8</i> E-01	5. 431 1 7E-06	1.09356E 03	-1,97009E-04	-5.518l4E-Q4	4.15475E 00	
286	4.58281E 00	1.93021E 00	3.72890E-01	5.42326E- 3 6	1.09366E 03	-1,27160E-DS	-8.71943E-04	4.15583E 00	
289	4.373246 00	2.36633E 00	3.94153E-01	5.441496-06	1.093446 03	1. 9 6512E-04	-1.097786-03	4.15335E 00	
290	4-10207E 00	2.81037E 00	3.04206E-01	5.442252-06	1.09343E 03	-6.62768E-04	3.48690E-04	4.15324F 00	YES
291	3.79435E 00	3.21412E 00	3, Q 4262E-\$1	5.44307E-96	1.093426 03	-1 -12565E-03	7.87177E-B4	4-15314E 00	YES
29 2	3.45528E 00	3.57518E 00	3-04677E-01	5 <u>.</u> 449056-06	1.09335E 03	-1.076215-03	5.57202E-04	4.152328 00	YES
293	3.08629E 00	3.89814E 00	3.04759E-01	5 . 45024E-06	1.09334E 03	-9.636902-04	3.21459E-04	4.15216E 00	
294	Z.68744E 00	4.18423E Q0	3.34988E-01	5.453536-06	1.09330E 03	-7.55923E-04	7.248246-05	4.15171E 00	YES
295	2.25970E 00	4.43016E 00	3.05255E-01	5.45739E-06	1-09326E 03	-6.14970E-04	-7.700038-05	4.151198 00	YES
296	1.80946E QQ	4,63200E 00	3.05252F-01	5.45778E-06	1.09325E 03	-1.54991E-Q4	-3.13014E-D4	4.15114F 00	YES
297	1.34950E 00	4.78694E D7	3.05231E-01	5.45704E-06	1.093266 03	9.01252E-04	-6.19671E-04	4.15124E 00	YES
298	8.71825E-01	4.855318 00	3.05123E-01	5.45548E-06	1.09328E 03	1.20705E-03	-5.69218E-04	4.151456 00	YES
299	3.69772E-01	4.95877E 00	3.05163E-01	5.45605E-06	1.09327E 03	4.36729E-04	-3.79649E-04	4.15137E 00	YES
300	-1.45519E-01	4.97057E 00	3.05224E-01	5.45694E-06	1.093265 03	-8.25527E-04	-3.69400E-04	4.15125E 00	YES

MACH 4 NOZZLE (G=1.24)

ZE = 2.40000F 91

STEP NO. 78

NO. φ AHO THETA P\$1 ü BODY -6.32573E-01 4.9324LE 00 3.05269E-01 5.45758E-06 1-09326E 03 -9.48742E-04 -4.58292E-04 4.15117E DO YES 302 -1.11277E 00 4-846826 00 3.05367E-01 5-45900E-06 1.09324E 03 -9.03791E-04 -5-62772E-04 4.15097E 00 YES 303 -1.5831CE 00 4.714345 00 3.05222E-01 5. 45691 E-06 1.09326E 03 -8-57809E-04 -6.51248E-04 4-15126E 00 304 -2.04200E 00 4.53442E 00 3.05259E-01 5.45744E-06 1.09326E 03 -7-14642E-04 -6.98896E-04 4.15118E 00 YES 306 -2.48387E 00 4.30803E 00 3.05195E-01 5.45652E-06 1.093270 03 -2.98464E-Q4 -5.69335E-04 4.151316 00 YES 336 -2.89476E DO 4.04243E 00 3.048836-01 5-452726-06 1-09332E 03 7-41958E-04 1.104212-04 4.15192E 00 307 -3.27734E 00 3.73863E 00 J. 04997E-01 5-45367E-06 1.09330E 03 1-31809E-03 7.01400E-04 4.15170E 00 306 -3.63365E QQ 3.39416E 00 3. 04772E-01 5.45042E-06 1.09334E 03 1-17344E-03 7.5426E-04 4.15214E 00 309 -3.95812E 00 3.70988E 09 3-94763E-01 5-43028E-06 1-09334E 03 6.17461E-D4 2.46134F-04 4.15215E 00 310 -4.23996E 00 2.59783E 00 3.04764E-01 5.450J0E-06 1.09334E 03 1.85128E-04 -3.50903E-04 4.15215E 00 311 -4.47996E 00 2.158236 00 3.04604E-01 5.44799E-06 1.09337E 03 3.75457E-05 -7.051346-04 4.15246E 0D 312 -4.67374E 00 1.89916€ 00 3.04491E-01 5.44636E-06 1.79339E 03 7.37672E-07 -9.88238F-04 4.15269E 00 313 -4.BI955E 00 1.22505E 00 3.04356E-01 5.44442E-06 1.09341E 03 5.92613E-05 -1.14376E-03 4.15295E 00 714 -4.91780E 00 7.368398-01 J. 04478E-01 5.44618E-06 1.09339E 03 1.51867E-04 -1.27813E-03 4.15271E 00 315 -4.96693E 00 2.39795E-01 J. 04665E-01 5.44888E-06 1.09336E 93 2.93092E-04 -9.66645E-04 4.15235E 00 316 -4.96645E 00 -2.49564E-01 3.00435E-01 5.44556E-06 1.09340E 03 3.22801E-04 3-34887E-04 4.15279E 00 317 -4.91767E 00 -7.37968E-01 3.04600E-01 5.44793E-06 1,09337E 03 1-69576E-04 1.16412E-03 4.15247E 00 316 -4.81937E DO -1.22508E 00 3.04473E-91 5-446L9E-06 1-79339E 93 9-65620E-06 1.33673E-03 4.15272E 00 319 -4.67289E 00 -1.69980E 00 3.04775E-01 5.450476-06 1.09334E 03 -1-09537E-04 1-290908-03 4.15213E 00 320 -4.47938E QQ -2.15951E OD 3.05030E-01 5.45414E-06 1.09330E 03 -5.76118E-05 8.98178E-04 4.15163E 00 321 -4.23937E DO -2.59918E 00 3.05314E-01 5.45823E-D6 1-09325E 03 1.33941E-04 4.28973E-04 4.15108E 00 322 -3.95717E 00 -3.01047E 00 3.05306E-01 5-45B12E-06 1.09325E 03 6,00306E-04 -2.29220E-04 4.15109E 00 323 -3.63285E 00 -3.39464E 00 3.05358E-01 5.45887E-06 1.09324E 93 1.16426E-03 -7.53246E-04 4.15099E 00 324 -3.27701E 00 -3.73978E 00 3.05659E-01 5.46321E-06 1.09319E 03 1.34061E-03 -7.23631E-04 4.15040E 00 325 -2.89373E 00 -4.04372E 00 3.05504E-01 5.46097E-06 1.09322E 03 8-02797E-04 -1.55613E-04 4.15070E 00 326 -2,48179E 00 -4.30875E 00 3.05738E-01 5.46435E-06 1.09318E 03 -2.14848E-04 5.19614E-04 4.15025E 00 327 -2.03981E 00 -4.53576E DD 3,05793E-01 5.46514E-06 1-09317E 03 -6.35124E-04 6.620358-04 4.15014E 00 320 -1.58174E 00 -4.71534E 00 3.0574@E-01 5.46437E-06 1.09318E 03 -8.25739E-04 6-39102E-04 4-15025E 00 3 29 -1.11575E 00 -4.84610E 00 3.05717E-01 5.46404E-06 1.093186 03 -9.36661E-04 5.67348E-D4 4.150292 00 330 -6.36084E-01 -4.93162E 00 3.05757E-01 5.46462E-06 1.00317E 0J -3.45609E-04 3.90657E-04 4-15021E 00 331 -1.42147E-01 -4-97009E 00 3.05134E-01 5.455646-06 1.09328E 03 3.43636E-04 3-353476-04 4-15143E 00 3 32 3466029E-01 -4.95871E 00 3.053226-01 5.45835E-06 1.09325E 03 8.56509E-04 4.09230E-04 4.151062 OD. YES 333 8.68B45E-01 -4.89616E OB 3.04992E-01 5.45360E-06 1.09330E 03 1.332925-03 5.85812E-04 4.15170E 00 334 1.34977E 00 -4.78603E 00 3.049936-01 5.45361E-06 1-09330E 03 8-95645E-04 6-116236-04 4-15170E 00 335 1.81054E 00 -4.63149E 00 3.050578-01 5.45453E-06 1.09329E 03 -1-17678E-04 3-26286E-04 4-151585 00 336 2.25941E 00 -4.43010E 00 3.04874E-01 5.45189E-06 1.093328 03 -6-13119E-04 7.71187E-05 4-15194E 00 337 2.68655E 00 -4.18475E OD 3.04652E-01 5.44869E-06 1.09336E 03 -8.23262E-04 -1.14736E-04 4.15237E 00 338 3.085500 00 -3.89932E 06 3.04407E-01 5.445|5E-06 4.15265E 00 1.09340E 03 -1.03858E-03 -3.91975E-04 339 3.454AZE 00 -3.57631E OD 3.04355E-0L 5.4444BE-06 1-09341E 03 -1-19741E-03 -6+695Cat-04 4.15295E 00 340 3.79389E Q0 -3.21509E 30 3.03941E-01 5.43843E-06 1-0934EE 03 -1.24832E-03 -9.29814E-04 4-15376E 00 341 4.10187E 00 -2.61117E 00 3.03999E-01 5.43797E-06 1.09348E 03 -7-68471E-94 -5.0Ze32E-04 4.15383E 00 342 4.37311E 00 -2.36708E 00 3.03921E-01 5.43814E-06 1.09348E 03 1.17415E-04 9.51996E-04 4.15385E \$7 343 4.58270E 00 -1.93070E 00 3-02732E-01 5. 42099 E-06 1+0936BE 03 -7-62651E-05 7.26741E-04 4-15614E 00 - YES 344 4.75201E 00 -1.46527E 00 5.42960E-06 3.03329E-01 1.09358E 03 -2.49965E-04 3-89101E-04 4.15496E 00 345 4.87435E 00 -9.83505E-61 7.0331 6E-01 5.42942E-06 1.09358E 03 -3.17399E-04 2.13965E-04 4-15499E 00 YES 346 4.94792E 00 -4.94316E-01 3.03261E-01 5.42861E-06 1.09359E 03 -3.46455E-04 8-45271E-05 4.1551 DE 00 YES

5. 451 89E-06

1.09332E 63

-6.13119E-04

7.71187E-05

4-15194E 00

-

336

2.25941E 00

-4.4301GE 00

3-048746-01

337	2.48655E 00	-4.16475E 00	3.04652E-01	B. 44869E-06	1.09336E 03	-0.232626-04	-1.14736E-04	4-15237E DD
338	3.08559E QU	-3.699322 00	3-04407E-01	5,44515E-06	1.09340E 03	-1.056562-03	-3.91975E-04	4-15255E 00
339	3.45462E 00	-3.57631E 00	3,04365E-01	5.44440E-96	1-09341E 03	-1-197416-03	-6.6950BE-04	4-15295E 00
340	3.79389E 00	-3.21509E 00	3.03941E-01	5.43843E-Q6	1.893488 63	-1-24032E-03	-9.29814E-04	4.15376E 00
341	4-10107E 00	-2:81117E 00	3.03909E-01	5. 43797E-06	1.0934BE 03	-7-684716-04	-5.02632E-04	4-15383E DO
342	4.37311E DO	-2.36708E 00	3.039214-01	5.43614E-06	1.0934BE 63	1.17415E-04	9-519985-04	4.15360E 00
343	4.5827QE 00	-1.93070E 00	3.027J2E-01	5.42099E-06	1.09368E 03	-7.02651E-05	7.2674LE-04	4.15614E 00
344	4.752012 00	-1.46527E 00	3.033296-01	5.42960E-06	1.0935BE 03	-2.499656-04	3.891 01E-04.	4-15496E DD
345	4.074382 00	-9.83505E-01	3-03310E-01	5. 42942E-96	1.09350E 03	-3.173996-04	2.139655-04	4.15499E 00
346	4.94792E 00	-4.94316E-01	3.03261E-01	5, 4286) E-06	1.09389E 03	-3.46455€-04	0.4587LE-05	4.1551 DE 00

NOMENCLATURE

- a Speed of sound
- h Static enthalpy
- L Distance along bicharacteristic
- \vec{L} , \vec{M} , \vec{N} Bicharacteristic coordinate system
- M Mach number
- n_1 , n_2 , n_3 Unit normal to body surface in z, x, y directions
- p Pressure
- q Velocity
- <u>q</u> | <u>q</u> |
- r* Throat radius of axisymmetric nozzle
- R Gas constant
- T Temperature
- u x component of velocity
- v y component of velocity
- w z component of velocity
- x, y, z Cartesian coordinate system

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- β Mach angle
- γ Ratio of specific heats
- δ Parametric angle for bicharacteristic
- θ , ψ Flow angles defined in Fig. 1
- ρ **Density**

SUBSCRIPTS

- i = 1, 2, ... refer to quantities at given points
- ts Stagnation conditions along streamline